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by


KEVIN M. BOYLE

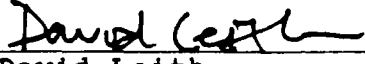
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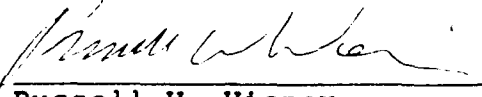
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## ABSTRACT

### Numerical Calculation of Aspiration Efficiency of Aerosols into Thin Walled Sampling Inlets.

Efficiency of aspiration of particles from a flowing airstream into a thin walled sampling inlet is accurately predicted using a numerical model. The model combines the Boundary Integral Equation Method for predicting the air velocity field into the inlet with an analytical solution to the particle equations of motion to describe particle trajectories. A two and a three dimensional model are examined. Results for the three dimensional model correlate well with an empirical model of aspiration efficiency. The method can be generalized for a wide range of airstream, sampling inlet, and particle conditions.

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## TABLE OF CONTENTS

I.	BACKGROUND.....	1
II.	THEORY.....	7
III.	METHOD.....	13
IV.	RESULTS.....	31
V.	DISCUSSION.....	39
VI.	CONCLUSION.....	48
VII.	FUTURE WORK.....	49
VIII.	APPENDIX.....	53
IX.	REFERENCES.....	118

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# NUMERICAL CALCULATION OF INERTIAL ASPIRATION EFFICIENCY OF AEROSOLS INTO THIN-WALLED SAMPLING INLETS

by

Kevin M. Boyle

Unbiased sampling of airborne particulate from a flowing stream requires that the size distribution and concentration of aerosol collected be identical to that of the aerosol in the free stream. Sampling errors occur during aspiration of the aerosol from the free stream to the face of the inlet and during transmission of the aerosol along the sample tube. Additional losses or gains may occur due to particle bounce from the front edge of the sample tube. In this paper, a numerical model for determining the aspiration component of overall sampling efficiency for any arbitrarily shaped thin edged inlet is presented.

## BACKGROUND

Sampling errors due to aspiration occur when particles fail to enter the sampling inlet with the air. Particles have inertia which may prevent them from accelerating, decelerating, or changing their direction fast enough to move with the air (Agarwal and Liu, 1980). Particles also possess additional motion due to gravity. Aerosol aspiration efficiency,  $E_a$ , is defined in equation (1) as the ratio of particle concentration entering the sampling inlet,

$C_i$ , to the particle concentration at an undisturbed upstream location,  $C_o$ , (Belyaev and Levin, 1972).

$$E_a = \frac{C_i}{C_o} \quad (1)$$

One effect on aspiration efficiency would be loss or gains of particles due to bounce off the front of the sampling inlet. By modeling the system as a thin walled sampling inlet, particle rebound effects are assumed negligible and do not contribute to the overall aspiration efficiency (Belyaev and Levin, 1974).

Both numerical modeling and physical experiments have attempted to describe aspiration efficiency. Belyaev and Levin (1972, 1974) used flash illumination to photograph particle trajectories and develop equations to predict inertial aspiration efficiency. Durham and Lundgren (1980), developed aspiration equations from experimental data for aspiration efficiency during anisokinetic sampling with nozzle misalignment and sampler inlet velocity different from oncoming wind velocity. Their equations account for the projected area of the nozzle when it is misaligned. Jaysekera and Davies (1980) and Davies and Subari (1982) also performed experiments and derived aspiration equations which were similar to the equations of Belyaev and Levin.

Extensive measurements of sampling efficiency were made by Tufto and Willeke (1982), and Okazaki, Wiener, and Willeke (1987a, 1987b, 1987c) for both isoaxial and non-

isoaxial aerosol sampling conditions. Based on this data and work cited above, Hangal and Willeke (1990) proposed a unified model to predict aspiration efficiency,  $E_a$ . The general expression, equation(2), is:

$$E_a = 1 + (R \cos \theta - 1)f \quad (2)$$

where  $R$  is the velocity ratio,  $\theta$  is the sampling angle and  $f$  is an inertial parameter. For the case of  $0^\circ$  sampling angle the inertial parameter,  $f$ , is based on the work of Belyaev and Levin (1974) and is shown in equation (3).

$$f = 1 - 1 / [1 + (2 + 0.617/R) Stk] \quad (3)$$

$$R = U_o/U_i$$

$U_o$  is the free stream velocity

$U_i$  is the inlet velocity

$Stk$  is the Stokes number

For  $0^\circ$  to  $60^\circ$  sampling angle the parameter is based on the work of Durham and Lundgren (1980), equation (4).

$$f = \frac{[1 - 1/[1 + (2 + 0.617/R)stk']]}{[1 - 1/[1 + 0.55stk' \exp(0.25stk')]]} / [1 - 1/[1 + (2.617)stk']] \quad (4)$$

where

$$stk' = Stk \exp (0.022\theta) \quad (5)$$

To model the movement of particles in air it is necessary to model the airflow field and derive a method to track particles placed in the air stream. (Agarwal and Liu,

1980). Numerical models of air flow fields and particle trajectory paths have been developed by Agarwal and Liu (1980), Addlesee (1980), and Dunnett and Ingham (1986, 1988). Agarwal and Liu determined the theoretical flow field into a thin walled sampling inlet considering both particle inertia and gravitational settling. A numerical calculation procedure was used to solve the axisymmetric Navier-Stokes equations and particle motion equations.

Addlesee, (1980) studied the intake efficiency of a Casella cascade impactor. The impactor was modeled as a two dimensional infinite slot with no end effects. A solution to the flow field was developed by assuming that viscous forces were not significant and calculating stream lines using potential theory. From the flow field developed, the particle equations of motion were solved assuming that Stokes law is applicable ( $Re < 1$ ). The equations were put into finite difference form and solved by relaxation.

Dunnett and Ingham (1986) developed a mathematical theory to predict aspiration efficiency of two dimensional blunt bodies using the Boundary Integral Equation Method. Once the velocity field of the system was known, the particle equations of motion are solved assuming that the Reynolds number is always less than 1.0 and thus Stokes' drag could be applied. The equations were put in finite difference form and solved numerically. In 1988 they expanded the two dimensional solution to an axisymmetric blunt body sampler and numerically predicted aspiration

efficiency by particle tracking using finite difference techniques.

Flynn and Miller (1989) used the boundary integral equation method to model air flow into local exhaust hoods. Their solutions follow the same logic as Dunnett and Ingham and give good agreement with analytic solutions for flow into an infinitely flanged rectangular hood with a constant velocity at the hood face, and with other empirical models. The advantage of their model was that it reduced a 3 dimensional air flow solution to a 2D area solution along the boundary of a specified domain.

This research employs the model of Flynn and Miller to estimate the air flow into a sampler inlet, and then applies the solution for the particle equations of motion developed by Alenius (1989) to determine aspiration efficiency. The particle motion equations are described in the THEORY section which follows.

The referenced numerical models to calculate aspiration efficiency were limited by the geometry of the solution domain and employed finite difference techniques to solve the particle equations of motion. By combining the 3D airflow solution of Flynn and Miller with the analytic solution to the equations of motion proposed by Alenius (1989), this model can calculate particle trajectories into a thin edged inlet. This model has a significant advantage over other models as it does not require finite difference discretization to calculate particle trajectories and has

the flexibility to be developed for any arbitrarily shaped domain and sampling inlet over a wide range of particle size and velocity conditions.

## THEORY

To model particle flow, a method for determining the characteristics of the flow field into an arbitrarily shaped and oriented sampling inlet is required. Once the flow field is described, particles can be placed into the field, assigned initial conditions, and tracked. From the trajectories, an estimate of the aspiration efficiency can be made and compared with previous models or experimental data.

The boundary integral equation method (BIEM) is a method of solving a potential flow problem for any arbitrarily shaped domain. The assumptions in the development are inviscid, incompressible, irrotational flow which leads to the following expressions:

$$\text{grad} \cdot \mathbf{V} = 0 \quad (\text{continuity equation for incompressible flow}), \quad (6)$$

and;

$$\text{curl } \mathbf{V} = 0 \quad (\text{irrotational flow}). \quad (7)$$

Irrotational vector fields possess a potential function such that the vector is equal to the gradient of the potential,  $\phi$ , and thus

$$\mathbf{V} = \text{grad } \phi. \quad (8)$$

By combining the above equations

$$\begin{aligned} \text{grad} \cdot \mathbf{V} &= \text{grad} \cdot (\text{grad } \phi) \quad \text{or} \\ \text{grad}^2 \phi &= 0 \end{aligned} \quad (9)$$

Equation (9) is Laplace's equation. By applying the divergence theorem and Green's second identity, an equation can be derived which relates the velocity potential at any singular point (P) to the potential and normal derivatives of potential along the boundary of a specified domain.

The derivation (Liggett and Liu, 1983) yields the following equations which form the basis of the Boundary Integral Equation Method for two and three dimensional domains.

$$2D: \alpha\phi(P) = \int_{\Gamma} [(\phi/R) \delta R/\delta n - ((1/R) \delta\phi/\delta n)] dS \quad (10)$$

$$3D: -\alpha\phi(P) = \int_{\Omega} [(\phi(\delta(1/R)/\delta n)) - ((1/R)\delta\phi/\delta n)] dA \quad (11)$$

- $\phi$  = velocity potential
- $\delta\phi/\delta n$  = velocity normal to the boundary
- $\alpha$  = solid angle about (P)
- $R$  = distance from singular point (P) to a point on the boundary.
- $\Gamma$  = closed curve surrounding and defining the 2D domain
- $\Omega$  = closed surface surrounding and defining the 3D domain
- $dS$  = differential element on  $\Gamma$
- $dA$  = differential area on  $\Omega$

The above equations can be written in discrete form in either two (Liggett and Liu, 1983) or three dimensions (Flynn and Miller, 1989). After specifying either  $\phi$  or  $\delta\phi/\delta n$  at each node on a discretized boundary of  $N$  nodes, equation (10) or (11) is written for each node by successively placing the singular point (P) at each node on the boundary. This results in a system of  $N$  equations in  $N$  unknowns which are solved simultaneously to give the unknown

value of  $\phi$  or  $\delta\phi/\delta n$  at each node on the boundary. Once the boundary values are known, (P) can be located at any internal location and the left hand side of equation (10) or (11) differentiated to give the velocity at the internal point.

Once the velocity field is determined, particles can be placed in the air stream and their motion tracked. This model uses an analytical solution to the particle equations of motion developed by Alenius (1989). The general form of the equation is:

$$d^2\mathbf{r}/dt^2 - [Q(Re)/\tau(\mathbf{u}-(d\mathbf{r}/dt))]-\mathbf{g} = 0 \quad (12)$$

where bold face variables denote vector quantities.

In the above equation, the following notation is used:

$d^2\mathbf{r}/dt^2$  ( $=d\mathbf{v}/dt$ ) is the acceleration of the particle

$Q(Re)$  is a dimensionless factor based on the Reynolds number and the drag coefficient

$\tau$  is the particle relaxation time in air

$\mathbf{u}$  is the air velocity at the particle location

$d\mathbf{r}/dt=\mathbf{v}$  is the velocity of the particle

$\mathbf{g}$  is the earth's gravity

$\mathbf{0}$  is the null vector

$\mathbf{r}$  is the particle position vector

The general equation presented is not analytically solvable. The reason is that the factor  $Q(Re)$  and the air

velocity  $u$  vary along the trajectory of the particle and thus indirectly with time  $t$ . If the air velocity at the points where the particle is successively located can be described as a linear function of the time that has elapsed and  $Q(Re)$  is assumed to be constant over the time interval, an analytical solution to the general equation can be obtained. This condition is approximately met if the motion of the particle is successively calculated using sufficiently small time intervals. A complete derivation is presented in the appendix. The analytic solution is:

$$v(t+t') = u_a t' + u_b - (u_b - v(t)) \exp[-Q(Re)t'/\tau] \quad (13)$$

$$r(t+t') = r(t) + u_a/2 t'^2 + u_b t' - (u_b - v(t)) \tau / Q(Re) (1 - \exp Q(Re)t'/\tau) \quad (14)$$

where  $t'$  is the size of the time step and  $u_a$  and  $u_b$  have been added to simplify the appearance of the equation:

$$u_a = (u(t) - u(t-t'))/t' \quad (15)$$

$$u_b = u(t) - (u_a - g)\tau / Q(Re). \quad (16)$$

Particles can now be tracked in any domain in which the air field is known, and the efficiency of aspiration determined. Aspiration efficiency is calculated as the ratio of particles entering the inlet to particles in the undisturbed flow field far upstream, equation (1). Figure 1 shows a conceptual stream tube of particles flowing in an

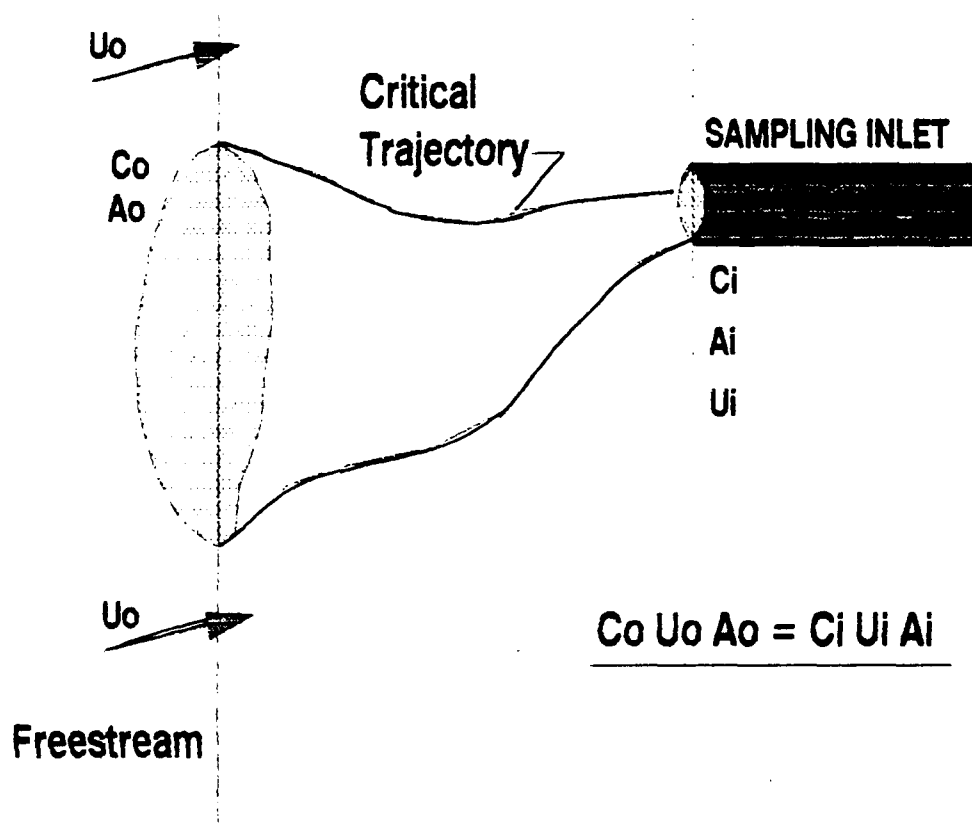


Figure 1. Conceptual Stream Tube. The flux of particles through the upstream plane equals that of particles passing the face of the sampler inlet.

airstream of given velocity,  $U_o$ , into an inlet sampling at a constant velocity,  $U_i$ . The boundaries of the stream tube represent all particle trajectories which just enter the tube. These trajectories are called critical trajectories. Particles located outside this tube would not be drawn into the inlet. The flux of particles passing through the upstream plane of the stream tube is particle concentration,  $C_o$ , multiplied by the stream tube cross sectional area,  $A_o$ , times the freestream velocity,  $U_o$ . By equating the flux of particles through the plane of the stream tube upstream from the inlet to that through the plane of the sampler face,  $C_i A_i U_i$ , the expression in equation (17) is obtained.

$$C_o A_o U_o = C_i A_i U_i \quad (17)$$

From equation (1),  $E_a = C_i/C_o$ , thus:

$$E_a = A_o U_o / A_i U_i \quad (18)$$

In equation (18), the characteristics of the sampler inlet,  $A_i$  and  $U_i$ , are known as well as the free stream velocity,  $U_o$ . By determining the coordinates of the critical trajectory start points in the free stream, an estimate of  $A_o$  and  $E_a$  can be made. This can be done by iteratively assigning particle locations in the free stream and tracking each particle in the domain until the critical trajectories are located.

## METHOD

The model was developed using a simple two dimensional problem which was then expanded to a more complex three dimensional case. Both isoaxial and non-isoaxial inlet orientations were modeled. Non-isoaxial conditions consisted of orienting the inlet at a pitch angle of  $30^\circ$  to the freestream.

### Two Dimensional Model

The two dimensional problem was modeled as an infinite slot. The coordinate system to visualize in two dimensions is an x-y cartesian system with the origin located at the center of the inlet. The positive x direction extends along the centerline of the hood face and the y direction is up and down, with gravity acting in the -y direction.

The air flow into the slot was modeled using the boundary integral equation method which provided a solution everywhere on the boundary of the domain for the potential and the normal derivative of potential. From the boundary solution, the exact velocity components at any internal point were calculated.

A FORTRAN computer program for the two dimensional boundary integral equation solution, written by Liggett and Liu (1983), was used for the 2D solution. The program, called GM8, returned the boundary values and the local air velocity components within the domain needed to calculate particle trajectories. GM8 was combined with a subroutine

written to solve the Alenius solution to the equations of motion, (11) and (12), and track particles within the domain. Figure 2 shows the flow of logic in the program.

The boundary of the domain in the simple 2-D case is shown in figure 3. The origin of the coordinate axes are located at the center of the sampling inlet. The upper lower, front and rear boundaries of the domain are at a distance of 20 inlet diameters from the inlet face. The remaining boundary consists of a rectangular indentation to represent the sampling nozzle of diameter equal to its width.

In figure 3, the boundary conditions are marked. The upper, lower, and rear boundary are situated far enough away from the sampling inlet to have potential due exclusively to the free stream velocity, or:

$$\phi = U_{ox}(x) + U_{oy}(y) \quad (19)$$

where  $U_{ox}$  and  $U_{oy}$  are the magnitude of the free stream velocity components and  $x, y$  are the location coordinates. The boundary condition on the line opposite the hood face is  $\delta\phi/\delta n = U_{ox}$ , the free stream velocity normal to the surface. On the upper and lower edges of the sampling inlet the boundary conditions are  $\delta\phi/\delta n = 0$ , no flow through the walls of the nozzle. At the face of the inlet  $\delta\phi/\delta n$  is equal to sampling velocity,  $U_i$ .

For the situation where an inlet pitch angle was introduced, the domain was not rotated  $30^\circ$  and a new

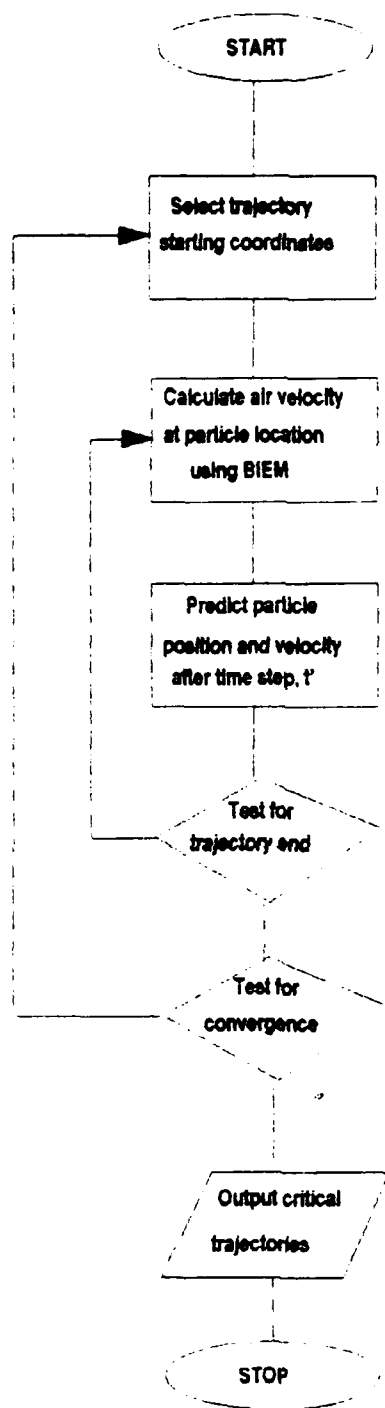


Figure 2. Flow diagram for the two dimension and 3 dimensional program logic.

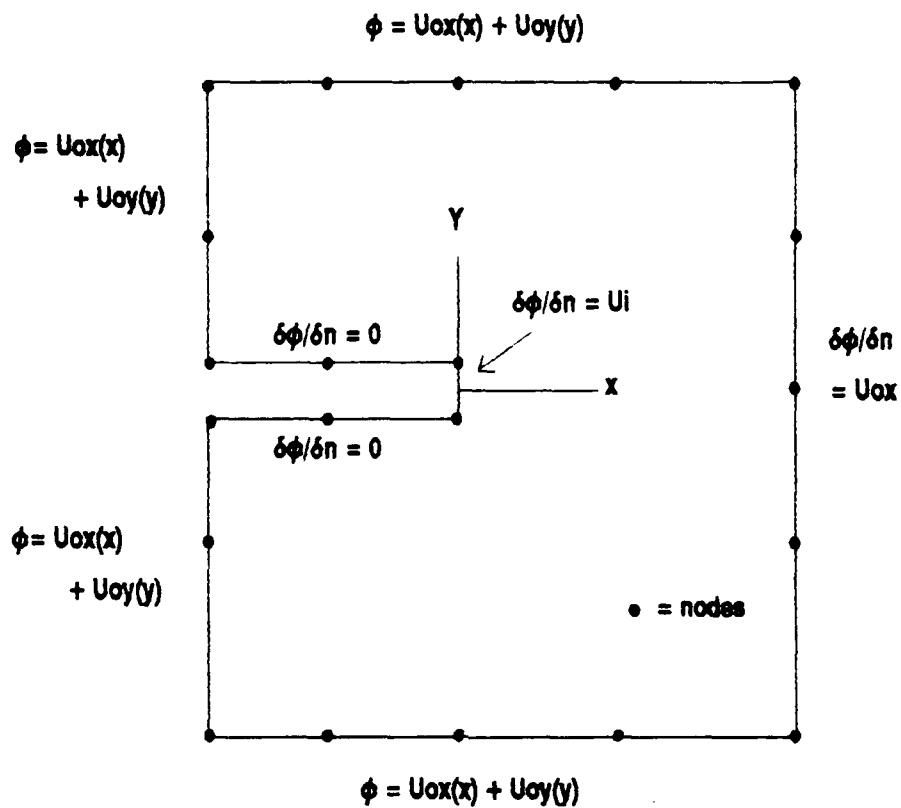


Figure 3. 2D model boundary with coordinate axes, boundary conditions, and sample discretization shown.  $\phi$  = potential,  $\delta\phi/\delta n$  = normal derivative of potential (air velocity).

boundary calculated. Rather boundary conditions were adjusted to represent the freestream,  $U_0$ , as the resultant of the free stream normal to the front boundary,  $U_{0x}$ , and a crossdraft,  $U_{0y}$ . This required a coordinate system conversion where the gravity vector in the x and y direction were  $-g \sin(\theta)$  and  $-g \cos(\theta)$  respectively,  $\theta$  was the angle of misalignment and  $g$  the magnitude of the gravity vector. The origin of this coordinate system was still centered at the inlet face.

The solution required the domain to be discretized into nodal elements as shown in figure 3. Much finer discretization than presented in the example is required because numerical accuracy during calculation of internal points suffers when the internal point is within 1 element length of the boundary.

The initial conditions assigned to the particles in the free stream are that they are falling at their terminal settling velocities and moving in the air stream (Addlesee, 1980) at the velocities calculated by the BIEM solution. Terminal settling velocity ( $V_{ts}$ ) was calculated using Stokes' Law:

$$V_{ts} = \tau g \quad (20)$$

where  $\tau$  is the particle relaxation time (Reist, 1984) and  $g$  is the acceleration due to gravity.

In two dimensions, it was necessary to define the location, in the free, stream of the upper and lower

critical trajectories to calculate aspiration efficiencies. This is because in two dimensions equation (18) reduces to:

$$Ea = d_o U_o / d_i U_i \quad (21)$$

where  $d_i$  is the inlet diameter, and  $d_o$  is the distance between the upper and lower critical trajectories. Internal air velocity coordinates were calculated using BIEM, then the particle position and velocity were predicted using the analytical solution and the process repeated. The critical trajectories were determined by selecting a point far upstream and tracking a particle from this point either into (capture) or past (miss) the inlet. Once a missed and captured trajectory were found the average of the two starting points determined the next point. Convergence occurred when the distance between the particle trajectory start point which is captured and that which escapes is less than a preset value. The program was designed to locate both an upper and lower critical trajectory corresponding to the upper and lower edges of the sampling inlet. The distance,  $s$ , between the upper and lower critical trajectories,  $d_o$ , was determined using the distance formula, equation (22).

$$s = ((x_1 - x_2)^2 + (y_1 - y_2)^2 + (z_1 - z_2)^2)^{1/2} \quad (22)$$

### Three Dimensional Model

In three dimensions,  $U_o$ ,  $A_i$ , and  $U_i$  are given and  $A_o$  is determined to calculate aspiration efficiency, equation (18).  $A_o$  is the area of the trajectory tube at an upstream location where the air flow is not influenced by the

sampling velocity. This area represents the boundary of the stream tube at an upstream location in which particles will enter the sampling inlet (Fig 1).

The shape of the three-dimensional domain is a square sided volume of half-width equal to 20 inlet widths. Extending from the rear wall of the volume into the center of the volume for a distance of 20 inlet widths is a sampling inlet with a square cross section. An equal area square is used to model a circular inlet to simplify the 3D boundary discretization.. The origin of the cartesian coordinate system is located at the center of the inlet. The x direction extends away from the hood face along its centerline. The z coordinate represents the height of the domain and the y coordinate represents the width.

For boundary conditions, the potential is specified on the front, rear, top, bottom and side faces of the 3D domain. The velocity is specified over the inlet face as  $U_i$ , and at the walls of the inlet tube as 0 cm/sec. As in 2D, the boundaries of the 3D domain are situated far enough away from the inlet to have potential due exclusively to the free stream:

$$\phi = U_{ox}(x) + U_{oz}(z) \quad (23)$$

Here,  $U_{ox}$  represents the velocity perpendicular to the front face of the domain and  $U_{oz}$  is the crossdraft vector used when the sampling angle did not equal zero. As in 2D, the gravity components in the coordinate system must be adjusted when a crossdraft is used to model the sampling angle.

The flow field is defined using the same theory as in two dimensions but using a FORTRAN program written by Flynn and Miller (1989) to solve the BIEM problem for three dimensions.

Particle trajectories were calculated in the same manner as in two dimensions with BIEM providing the local air velocity components at the particle location. The particles were assigned initial conditions as described in the 2D section and the equations of motion, with a third dimension added, were solved to predict the particle's next position and velocity. The program logic is the same as that shown in figure 2.

Because the domain is now in three dimensions, the region cannot be discretized into lines between nodes, rather, the boundary must be divided into areas. Flynn and Miller (1989) used triangular elements on the boundary. Examples of the discretization input files for the boundary are presented in the appendix.

The critical trajectories in 3D were determined by selecting a point far upstream and tracking a particle from this point either into the inlet (capture) or out of the domain (miss). The start point is a specified number of inlet diameters,  $XDIN$ , in front of the inlet and in the direction of the resultant velocity vector in the x-z plane. For  $0^\circ$ , this point is along the x axis at  $x=XDIN$ ,  $y=0$ ,  $z=0$ , because  $U_o = U_{ox}$  for this condition. For all other angles

the first trajectory start point, figure 4, is calculated as:

$$\begin{aligned}x &= XDIN \cos(\theta) \\y &= 0.0 \\z &= XDIN \sin(\theta)\end{aligned}\tag{24}$$

The rationale for choosing this start point is to obtain a capture trajectory around which starting points for the critical trajectories can be centered. If this first point does not yield a capture, the start point is incrementally adjusted up or down along a line perpendicular to the free stream and the trajectory is recalculated. The process is repeated until a first capture identified.

Once a capture trajectory is found, a series of start points at which to begin critical trajectories are defined at a distance far enough away from the coordinates of the first capture to have a high probability of a miss. These points are located a specified distance, AA, from the coordinates of the first capture ( $x_1, y_1, z_1$ ) in incremental degree steps,  $\alpha$ , around a semicircle in the plane perpendicular to the free stream, figure 5. Critical trajectories for only one half the area were calculated due to the symmetry of the problem.

The equations for these points are:

$$\begin{aligned}x &= x_1 + (AA \sin(\theta) \sin(\alpha)) \\y &= AA \cos(\alpha) \\z &= z_1 + (AA \cos(\theta) \sin(\alpha))\end{aligned}\tag{25}$$

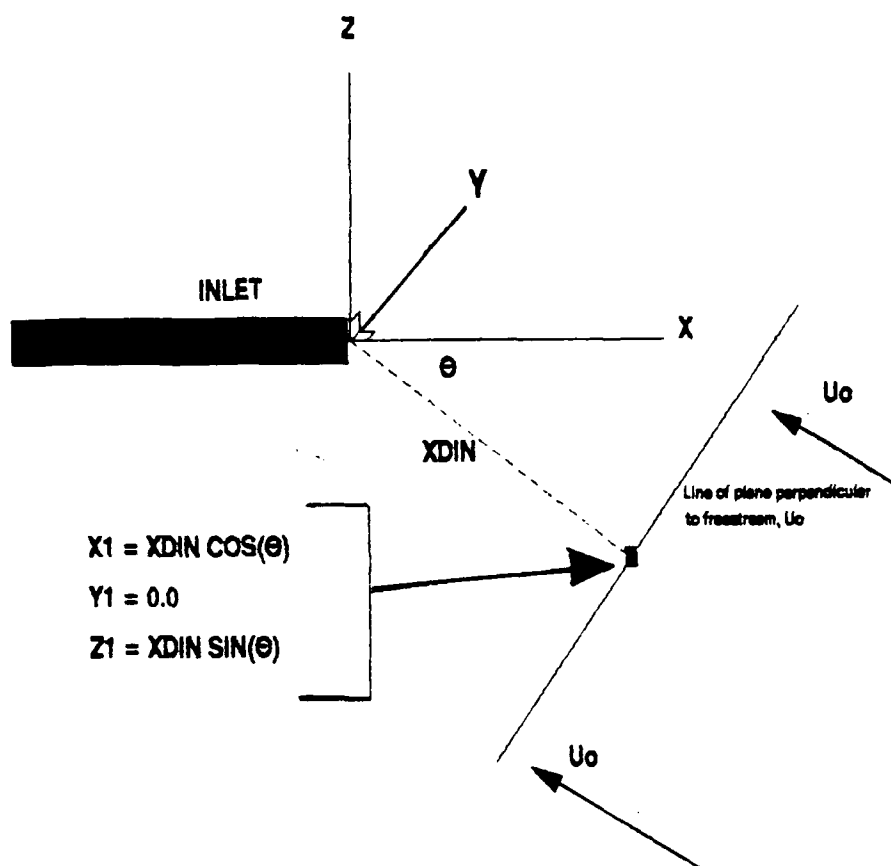
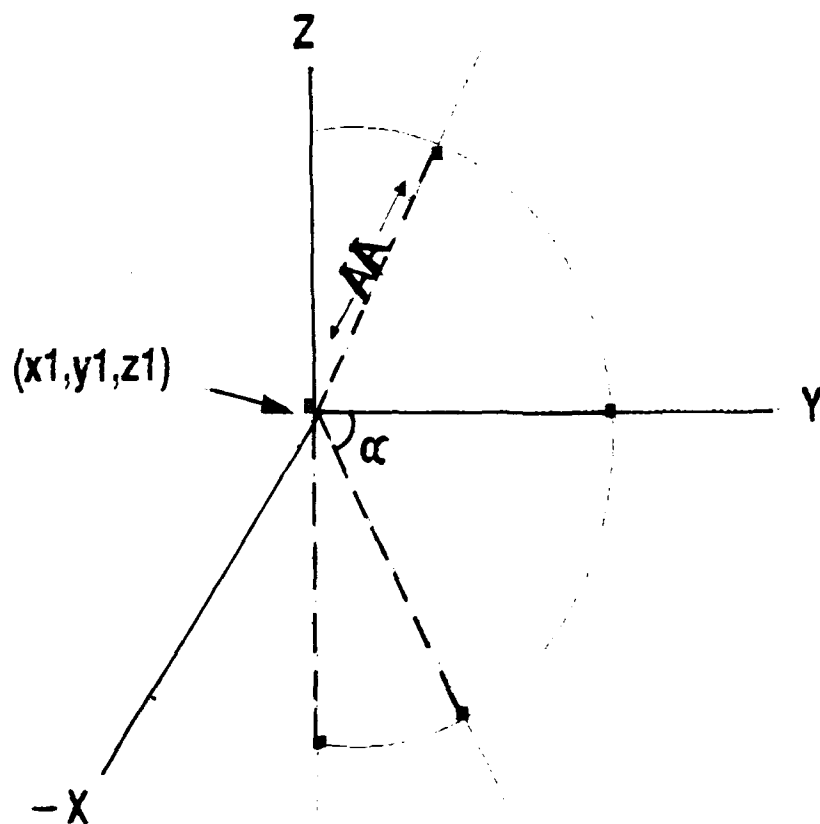


Figure 4. Location of initial trajectory start point.  $(X1, Y1, Z1)$  is initially placed at a distance  $XDIN$  in front of the inlet along a line perpendicular to  $U_0$  in the X-Z plane.



■ Trajectory start points

$$x = x1 + (AA \sin(\Theta) \sin(\alpha))$$

$$y = AA \cos(\alpha)$$

$$z = z1 + (AA \cos(\Theta) \sin(\alpha))$$

$\Theta$  = angle of misalignment

Figure 5. Trajectory start points are located on a semicircle centered around  $(X1, Y1, Z1)$  at degree increments,  $\alpha$ , along rays a distance  $AA$  from the center.  
 $(-90^\circ \leq \alpha \leq 90^\circ)$

If the start points defined in equation (25) result in a capture, the start point is incrementally adjusted farther from the initial capture point and the trajectory is recalculated until a miss identified.

Each first capture and initial miss coordinate combination results in a ray the end points of which define the upper and lower bounds of the critical trajectory and all rays are contained in the same plane perpendicular to the free stream. From this point, the starting coordinates of the last miss and last capture trajectory are averaged to determine the coordinates of the next start point on the ray. The process is repeated until the convergence criteria was satisfied. Critical trajectories are found for each starting point around the semicircle.

The output of the particle tracking routine is a series of points representing the critical trajectories which define  $A_o$ . The area,  $A_o$ , is calculated numerically with a FORTRAN program using the trapezoid rule. From  $A_o$ ,  $E_a$  is calculated using equation (18).

The models, both 2D and 3D, were verified by comparing the computed aspiration efficiency with the unified aspiration model proposed by Hangal and Willeke (1990), equation (2).

#### The Programs

The two dimensional program was compiled and run using Microsoft Fortran version 2. The entire aspiration efficiency calculation was run using one program. This

program initially calculates the boundary solution for the domain then calls subroutines to calculate particle velocity and position, and internal air velocity components at the particle's location. All 2D simulations were run on a Dell 386 personal computer and took approximately 15 minutes to complete. Each program run calculates approximately 30 separate trajectories with approximately 100 points calculated per trajectory.

Figure 6 shows an example of the output of the 2D program with particle positions plotted as trajectories. The particle trajectories were plotted using a simple routine written in BASIC (see appendix). The distance between the upper and lower critical trajectories was the basis of determining the aspiration efficiency as defined in equation (22). A commented version of the 2D program is contained in the appendix.

The 3D program is much more complex than the 2D version because of the addition of a third dimension and the resulting complexities of solving the BIEM equations. Because of this, 3D simulations were run on a Convex Super Computer. The 3D simulations were run using two FORTRAN programs. The first program, 4PTGQ.F, is the BIEM boundary solution program. The input for this program was a boundary node and element file for each combination of sampling velocity,  $U_i$ , wind velocity,  $U_o$ , and sampling angle,  $\theta$ . The input file contained 367 nodes,  $N$ , leading to  $N$  linear equations and  $N$  unknowns which were solved using a four

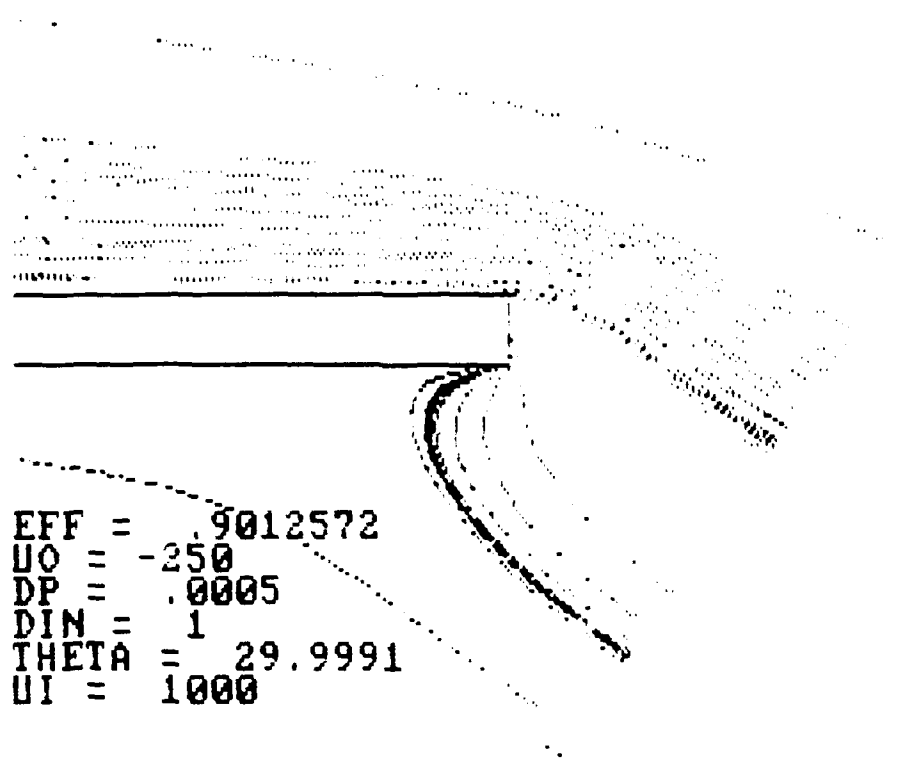


Figure 6. Sample of 2D trajectory plots. Trajectories originate in the plane of the freestream perpendicular to  $U_o$ .

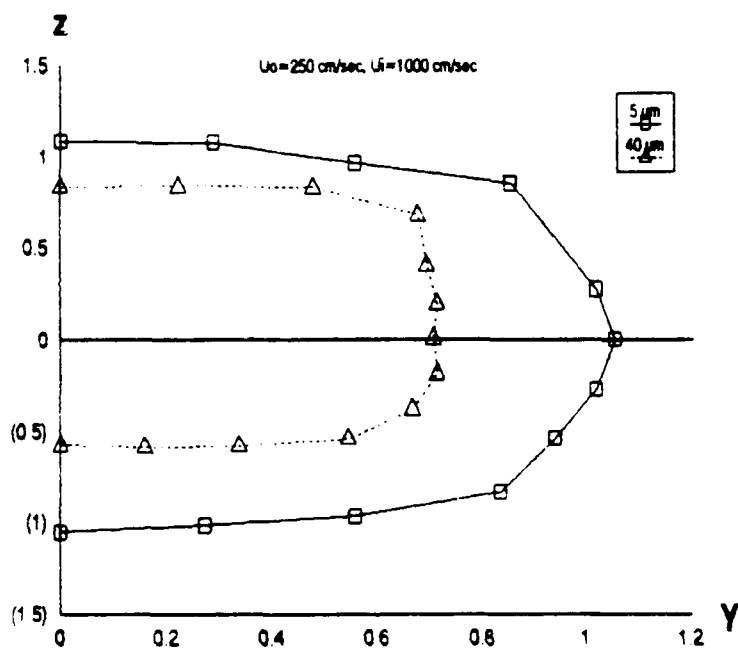
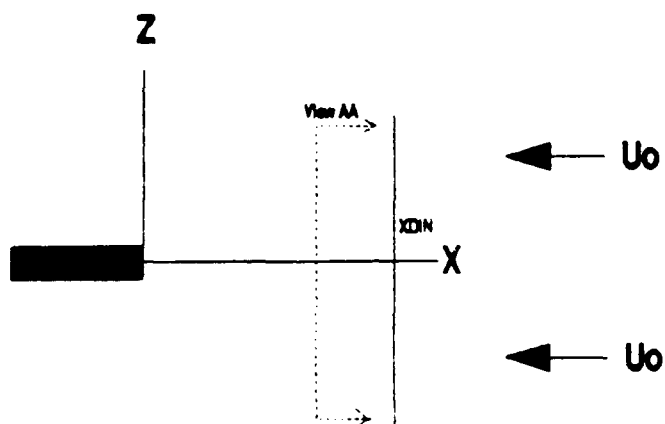
point gaussian quadrature. This program took 5.5 minutes to run on the Convex and returned potential and velocity values for each node on the boundary of the domain.

Once the output to 4PTGQ.F was received, it was imported as input to the 3D particle tracking program, TRK15.F. This program consists of a driver to specify particle location, test for convergence, and call subroutines to perform the BIEM internal air velocity, particle position, and particle velocity calculations. TRK15.F was designed to calculate 13 trajectories at  $15^\circ$  ( $\alpha = 15^\circ$  in equationkk (25)) increments around a semicircle surrounding the initial capture point (see figure 5). This leads to the calculation of approximately 10 trajectories per starting point, over the 13 starting points specified by the degree increment,  $\alpha$ , with 20-30 points along each trajectory to determine the fate of the particle. A typical combination of program variables shown below took 68 minutes of computer time on the Convex:

	$U_o =$	500 cm/sec
	$U_i =$	250 cm/sec
particle diameter	$=$	5 $\mu\text{m}$
	$\theta =$	30 degrees
time step	$=$	0.0005 seconds
convergence criteria	$=$	0.05 cm

The output of TRK15.F is a series of points which defines a region in the freestream inside of which all particles are aspirated to the face of the sampling inlet. Figures 7 and 8 show an example of the 3D model output.

## 3D Isoaxial Sample Output



Plot of critical trajectories  
in freestream, view AA.

Figure 7. Plot of critical trajectory start points in their starting plane. The area inside the curves is the estimate of  $A_0$  in equation (14). The area is assumed symmetrical about  $Z = 0.0$ .

## 3D Non-Isoaxial Sample Output

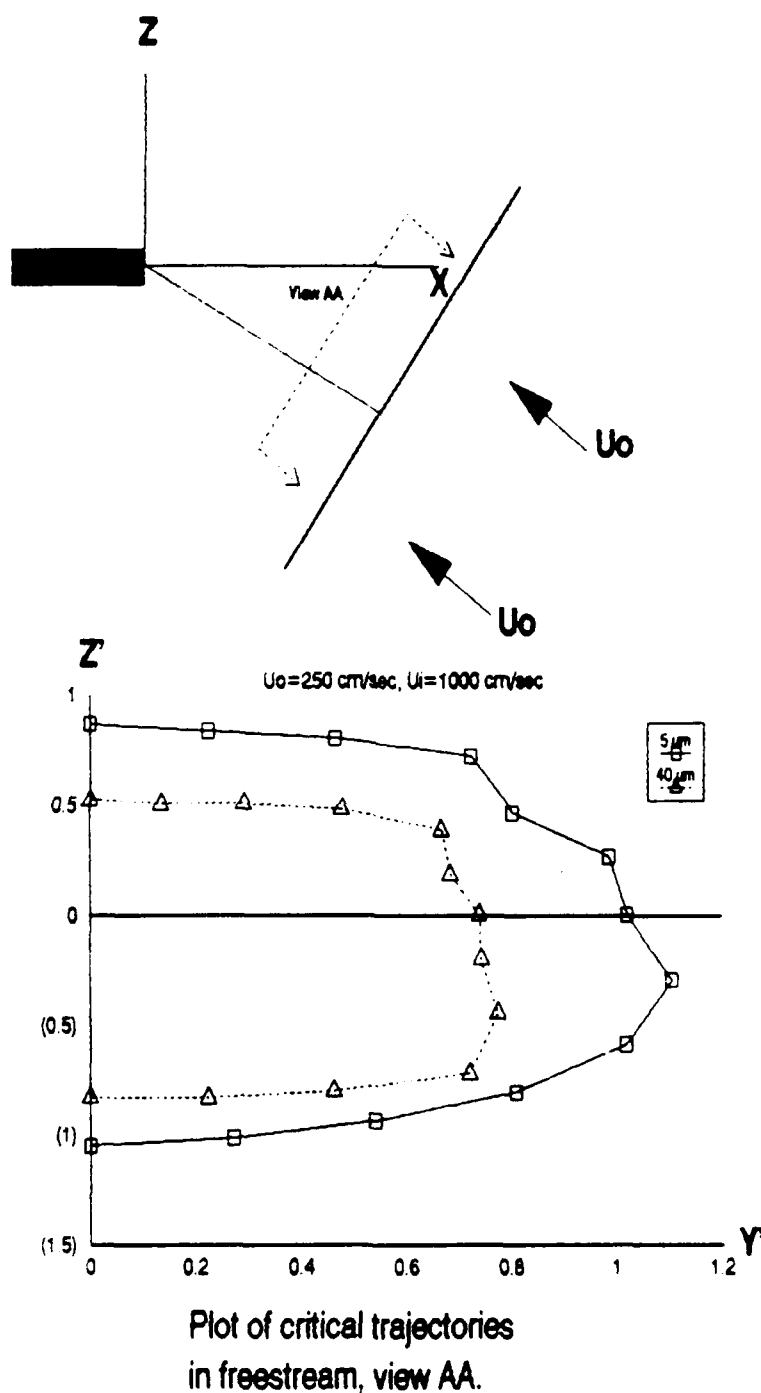


Figure 8. Plot of critical trajectory start point in their starting plane. The area inside the curves is the estimate of  $A_0$  in equation (14).  $Z'$ ,  $Y'$  represent the local coordinate system centered at  $(X_1, Y_1, Z_1)$ .

Figure 7 is an example of output for an isoaxial set of conditions. The plot consists of the location of the critical trajectories in the y-z plane at a constant value of x (distance in front of the sampling inlet) equal to XDIN in equation (24). In this case, x is constant because the sampling angle is 0° and the freestream is flowing in a direction perpendicular to the plane at  $x = XDIN$ .

The plot in figure 8 represents the area in the freestream,  $A_o$ , which is perpendicular to the freestream resultant velocity for the case when the sampling angle was 30°. In this case, a simple plot of the y-z coordinates would not represent the actual area of  $A_o$  as x was not constant over the plane of interest. To solve this problem the critical trajectory coordinates were converted to a local coordinate system centered around the coordinates of the initial capture point. First the distance, s, between the first capture point and the critical trajectory coordinate on each of the 13 rays defined by  $\alpha$ , the incremental angle, was calculated using the distance formula, equation (22). After the distances between the points were calculated, the x and y coordinates of the critical trajectories determined using the following relations:

$$Y' = s \cos \alpha \quad (26)$$

$$Z' = s \sin \alpha$$

The local coordinates were then used to numerically calculate the area using the FORTRAN program, AREA.F.

## RESULTS

Several combinations of free stream velocity,  $U_o$ , inlet size,  $d_i$ , inlet sampling velocity,  $U_i$ , sampling pitch angle (misalignment to the free stream), and particle aerodynamic diameter,  $d_{ae}$ , were run through the 2D and 3D programs.

Table 1 summarizes the input variables which coincide with input parameters used by Wiener (1987).

TABLE 1  
Model Input Parameters

$d_i$ cm	$U_o$ cm/sec	$U_i$ cm/sec	$d_{ae}$ micron	theta degrees
.32	250	125	5.0	0
1.0	500	250	40.0	30
	1000	500		
		1000		

The two dimensional program was run for 96 combinations of particle size ( $d_{ae}$ ), velocity ratio ( $U_o/U_i$ ), sampling angle ( $\theta$ ), and inlet diameter ( $d_i$ ). The results are summarized in the appendix.

A linear regression of the BIEM predicted aspiration efficiency on the empirical aspiration efficiency calculated from the unified aspiration model, equation (2), was performed for all 2D data collected, for all  $0^\circ$  combinations, and all  $30^\circ$  combinations. The results are summarized in table 2. Figures 9, 10, and 11 are plots of

the 2D aspiration simulation versus the unified aspiration model, equation (2).

TABLE 2

Two Dimensional Model Linear  
Regression Results

CATEGORY	SLOPE	Y INT	LCL (1)	UCL (2)	R <sup>2</sup> (3)
All Data	0.842	0.074	0.788	0.895	0.917
All 0°	0.963	0.077	0.941	0.986	0.993
All 30°	0.664	0.118	0.599	0.729	0.911

- (1) LCL - 95% lower confidence limit for slope  
 (2) UCL - 95% upper confidence limit for slope  
 (3) R<sup>2</sup> - correlation coefficient

The 3D results are presented in the appendix and summarized in figures 12, 13, and 14. Table 3 contains the linear regression results which compare the numerical prediction of aspiration efficiency with the unified model of Hangal and Willeke, 1990.

TABLE 3

Three Dimensional Model Linear  
Regression Results

CATEGORY	SLOPE	Y INT	LCL (1)	UCL (2)	R <sup>2</sup> (3)
All Data	1.062	-0.062	1.026	1.099	0.995
All 0°	1.059	-0.026	1.036	1.082	0.999
All 30°	1.064	-0.096	0.980	1.148	0.991

- (1) LCL - 95% lower confidence limit for slope  
 (2) UCL - 95% upper confidence limit for slope  
 (3) R<sup>2</sup> - correlation coefficient

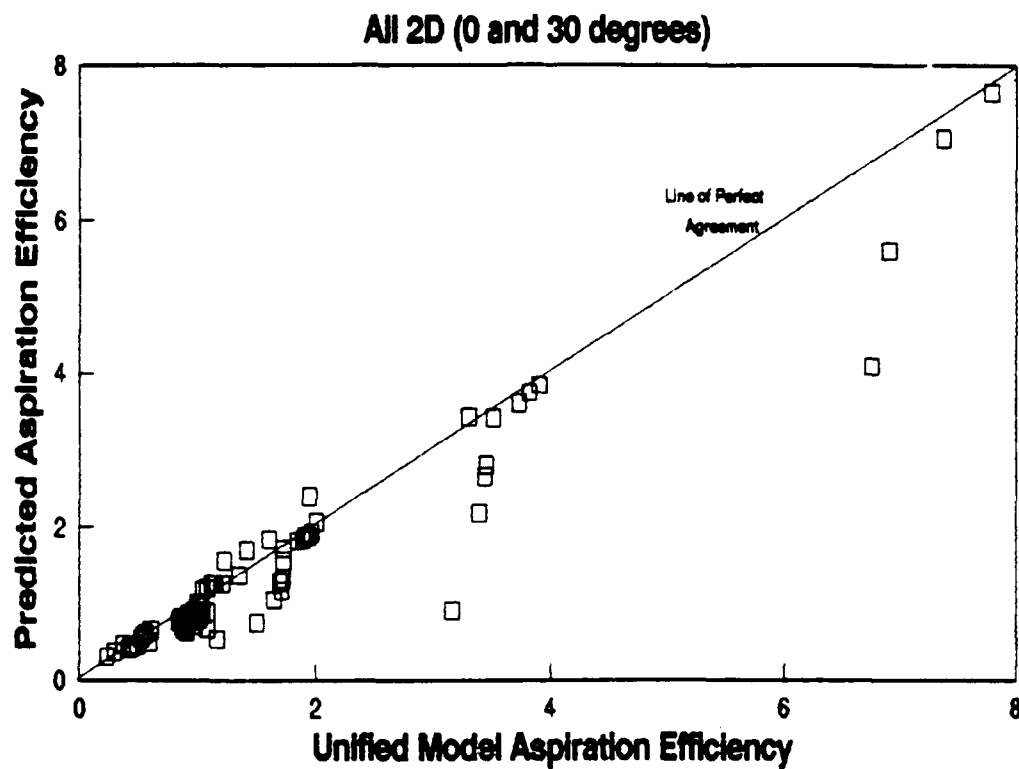


Figure 9. 2D results, all data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).

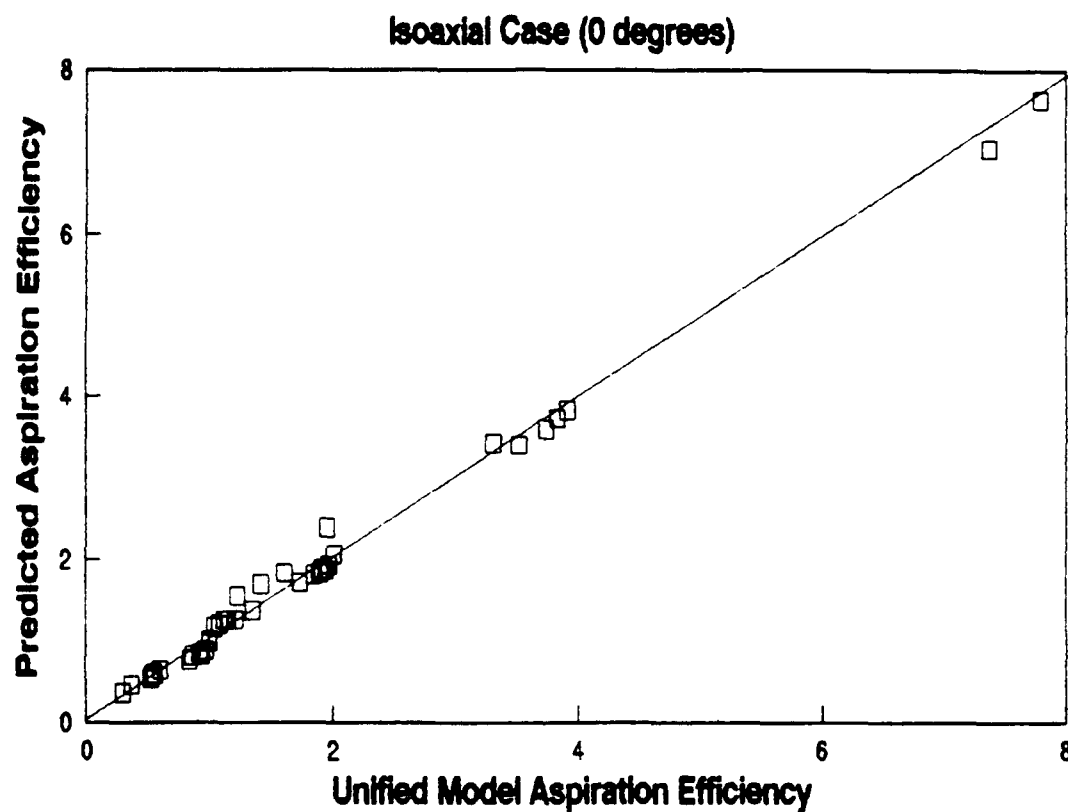


Figure 10. 2D results, isoaxial data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).

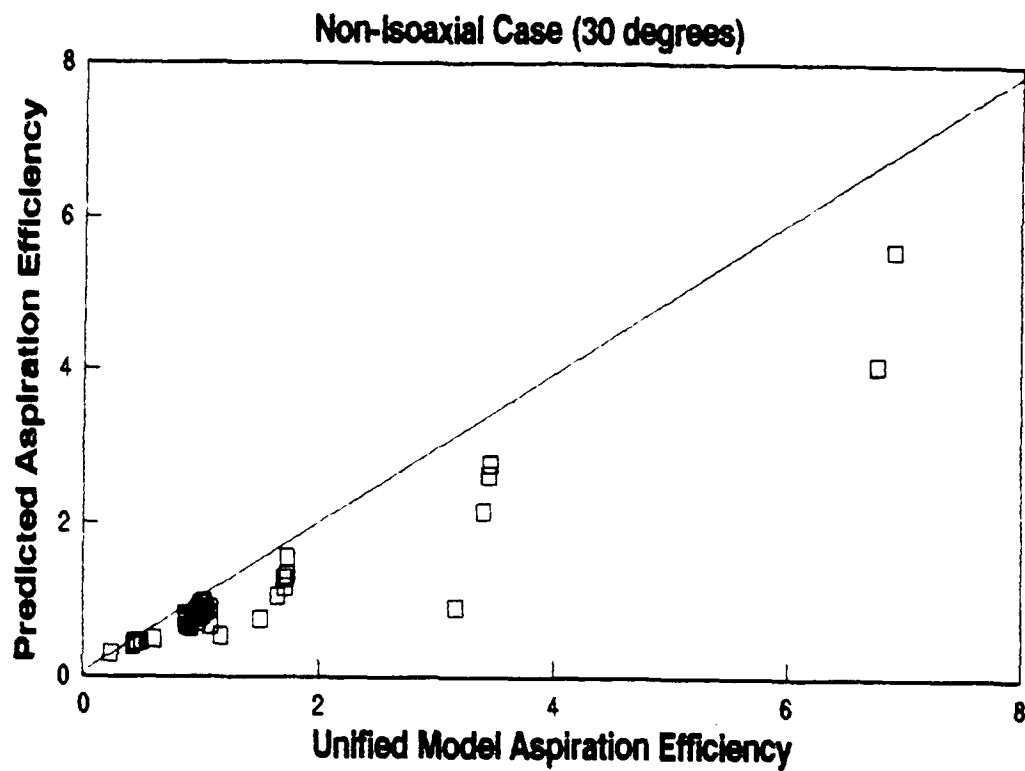


Figure 11. 2D results, non-isoaxial data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).

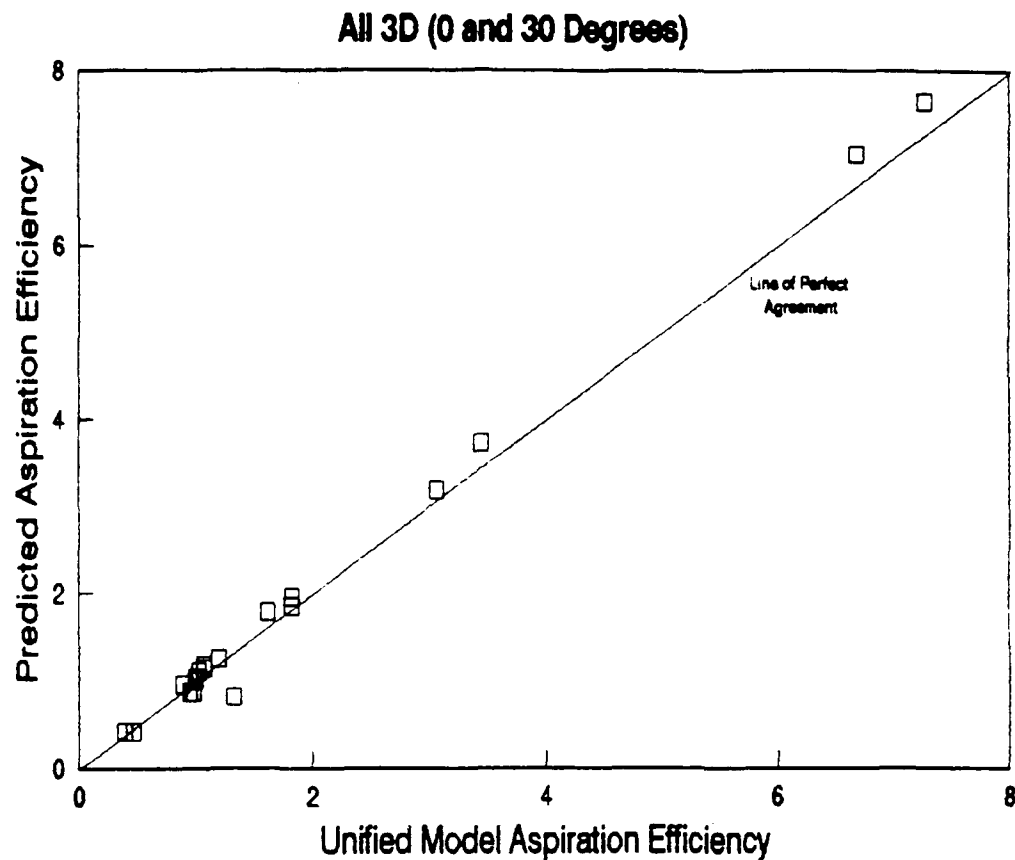


Figure 12. 3D results, all data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).

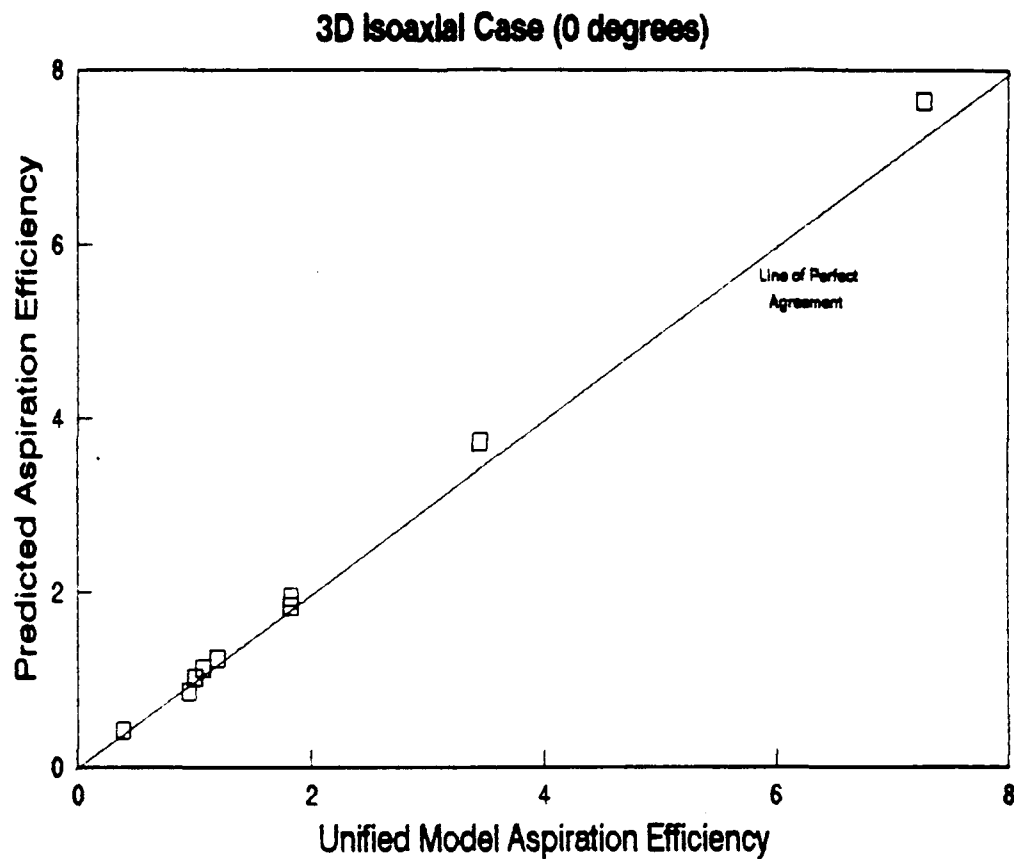
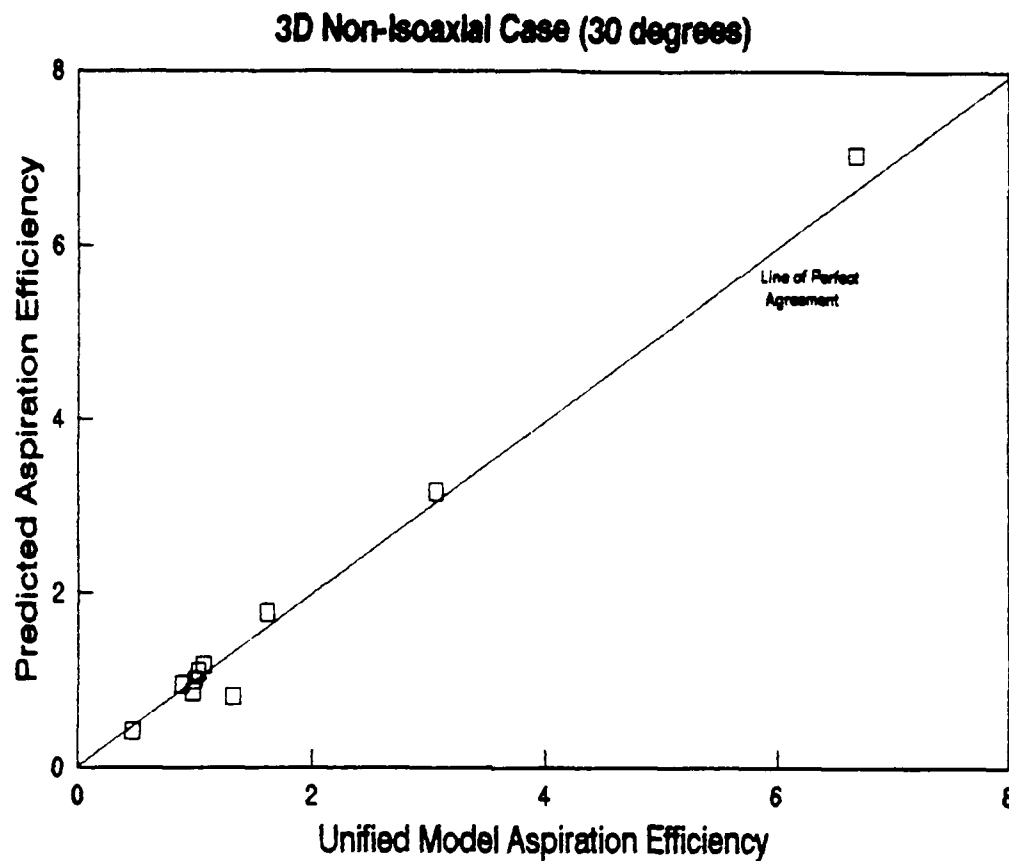


Figure 13. 3D results, isoaxial data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).



**Figure 14.** 3D results, non-isoaxial data. Plot of the predicted efficiency developed from the BIEM and Alenius theories against the empirical unified aspiration efficiency model of Hangal and Willeke (1990).

## DISCUSSION

The two dimensional model showed good agreement with the unified aspiration model for the isoaxial conditions. From table 2, the slope of the regression line for the  $0^\circ$  sampling angle is 0.96. A slope of 1.0 would indicate perfect agreement with the unified model. The largest error in the 2d model occurred when the velocity ratio was less than 1. In this case, the inlet velocity was 2 to 4 times greater than the wind velocity leading to large changes in air velocity and direction as the particles approached the inlet face.

The nonisoaxial 2D model was tested for a  $30^\circ$  sampling angle and showed poor agreement with the unified model. The percent difference between the unified model aspiration efficiency and the predicted aspiration efficiency was as large as -71%. The slope of the regression line for this set of conditions was .66.

Overall, the 2D model fairly represented the aspiration efficiency of aerosols into a thin edged inlet. The regression equation, slope of 0.84, was biased due to the poor agreement of the  $30^\circ$  model with the unified model.

As shown in table 3, the three dimensional solution performed significantly better in all categories when compared to the 2D model. The slopes of the regression lines were close to 1.0 for all cases indicating that the computer model accurately calculates aspiration efficiency

values when compared to the unified aspiration efficiency model. Table 4 shows a comparison of the 2D percent error with that of the 3D model for the same combinations of velocity ratios, sampling angle and particle diameter. As can be seen, in most cases, the 3D model led to an improvement in the aspiration efficiency value.

TABLE 4  
Comparison of 2D Model Error  
with the 3D Results

UO	UI	THETA	DP	2D ERR	3D ERR
1000	125	0	5	22%	2%
1000	125	0	40	4%	5%
250	1000	0	5	12%	-9%
250	1000	0	40	26%	9%
1000	125	30	40	-39%	5%
250	1000	30	5	-11%	-11%
250	1000	30	40	-3%	-10%
500	500	0	5	1%	3%
500	500	30	5	-10%	0%
500	250	0	5	11%	6%
500	250	30	5	-6%	7%
500	125	0	5	26%	4%
500	125	30	5	17%	10%

Some error was introduced into the above comparison because the unified model of aspiration efficiency was developed for circular, thin edged inlets. This may have some effect on the comparison of calculated efficiency with the aspiration efficiency derived from the computer. This does not, however, affect the model calculation of efficiency because the actual areas using the square inlet were used in equation (18).

Boundary discretization, particle start point, convergence criteria, and time step ( $t'$ ) were the most important parameters in determining accurate solutions. Boundary discretization had to be dense enough so that calculations of internal velocities were performed at distances greater than the distance between nodes on the nearest boundary (Flynn and Miller, 1989). This was accomplished by developing a 2D boundary consisting of 75 nodes with dense discretization near the inlet face and along the inlet sides. The appendix contains a sample input file for the 2D boundary discretization. With this discretization, few aberrations in internal velocity calculations were seen. This was not the case for the 3D solution.

The three dimensional model boundary discretization was proportional to the 2D discretization with the sides of the triangular elements equal in length to the distance between nodes in the 2D discretization. This led to an input file containing 367 nodes defining 693 elements. As described by Flynn and Miller, the triangular elements are defined by numbering the element with the node numbers corresponding to the vertices of the triangular element in a clockwise fashion looking out of the domain. This was done for approximately 1/2 of the elements starting at the inlet face and along the walls of the inlet using a triangular element generating program written for this problem. The remainder of the element input file was fashioned using

LOTUS spreadsheets because of the complex interactions of common nodes along the edges of each facet of the cube and at its corners.

Even with this dense 3D boundary discretization, internal calculation of air velocities at points less than 0.05 cm from the face and walls of the inlet were extremely inaccurate with the values being orders of magnitude larger than the freestream velocity. This led to large errors in the prediction of particle location which is dependent in part on accurate calculation of air velocity at the particle's current location. To avoid this error, capture criteria for the particle was extended by a factor of 0.05 cm in front of the inlet face and around its edges. This in effect enlarged the face area,  $A_i$ , to 1.11 cm<sup>2</sup> for a square inlet of side equal to 1.0 cm. This enlarged area was the area used in the aspiration efficiency equation (18).

The effect of enlarging this area was to alter the actual average air velocity moving into the "inlet". Over the face of the inlet the air velocity was specified as  $U_i$ . Over the thin layer defining the addition to the actual inlet, the average velocity had a value which was a function of the free stream velocity and the sampling velocity. Because of this there is some error in the specification of  $U_i$  in equation (184) and hence  $E_a$ .

Another problem with the 3D boundary discretization involves the interface of a surface of the boundary where the velocity is specified with another surface where the

velocity is also specified, but is different than that of the first surface. In the final model, this occurred only at the nodes surrounding the edges of the face of the sampling inlet. Here, the velocity over the face was specified as the sampling velocity,  $U_i$ , and the velocity on the edge of the tube and along its length was specified as 0 cm/sec. This caused a discontinuity of velocity at the edges of the sampling inlet. The effect of the discontinuity was to cause inaccuracies in interpolation of velocities over the elements involved. This interpolation error was minimized by inserting a very thin row of elements just inside the edges of the inlet. For the final model the width of this small layer was 0.001 cm.

Particle start points were important because the aspiration efficiency calculation requires the critical trajectory start points to be in the free stream. It was found that at distances of 6 inlet diameters from the inlet, local air velocity and direction was within 5% of the specified free stream velocity. This agrees with the findings of Belyaev and Levin (1972) and held true for both 2D and 3D models.

When determining the location of critical trajectories, the distance between the last capture trajectory start point and last miss trajectory start point was compared to the convergence criteria. Once the distance reached a preset criteria, the points were averaged to give the start point of the critical trajectory. The convergence criteria for

the 2D model was set at 0.01 cm after iterations at criteria smaller than this caused a less than 1% change in the calculated efficiency. The convergence criteria for the 3D model led to good agreement with the unified model when set at 0.05 cm.

The time step was the most critical factor in developing accurate particle trajectories. Time steps that were too large resulted in predictions of trajectories that were too coarse to accurately predict the particle movement. Unnecessarily small time steps caused excessive computing time. Through a series of program tests, 0.0003 seconds was chosen as the time step for the 2D model with a further reduction by a factor of 10 once the particle came within 1 inlet diameter of the sampling inlet to account for the large velocity changes near the face of the inlet.

The time step and the convergence criteria for the 3D model were not as sensitive in the determination of the aspiration efficiency as they were in the 2D case. Since the 3D model more realistically represented the physics of the problem, accurate solutions were obtained for time steps ranging from 0.001 to 0.0003 seconds with the time step being halved when the particle was within 1 inlet diameter of the inlet face.

Because the size of the time step indirectly predicts the distance the particle will move; positions predicted when the air is turning and accelerating will not lie on the the actual trajectory. This is clearly seen in the 3D model

for velocity ratios of 2 and 4 where the estimate of  $E_a$  was consistently larger than the unified model prediction. In this case, the air is approaching the inlet faster than the inlet is sampling and must diverge around the inlet.

Particle trajectories will also diverge but the predicted position will lie slightly inside of the actual trajectory. This causes an overestimate of  $A_o$  leading to an increase in the prediction of  $E_a$ .

When running the model under certain conditions, the time step and capture criteria became very critical in determining whether a trajectory resulted in a miss or capture. In the three dimensional model, when  $U_o = 1000$ ,  $U_i = 125$  cm/sec, and  $\theta = 30^\circ$ , the best estimate of aspiration efficiency was off by 39% when compared to the unified model. Under these conditions the air flow is approaching the inlet at 8 times the sampling rate causing significant divergence of the air streamlines around the face of the inlet. This situation combined with the sampling angle results in particle trajectories which move virtually straight up in the positive  $z$  direction at locations within 0.1 cm of the inlet face when the particle is approaching the inlet from above the centerline. The air velocity in this area is also moving very fast. The combination of high velocity particle and steep angle of approach toward the sample inlet can easily lead to a predicted particle location which jumps across the numerical edges of the sampling inlet. A miss trajectory is recorded for this

situation when in actuality a capture should have occurred. This causes an underestimation of  $A_o$  leading to a prediction of  $E_a$  which is too small. This situation occurred for the last four rays around the start point semicircle and is the reason for the poor performance of the model under these conditions. This situation can be eliminated by reducing the size of the time step but would lead to a large increase in computing. The same problem was seen in the 2D model and prevented identification of an upper critical trajectory.

By specifying an incremental angle of  $15^\circ$  in the 3D model, the program was limited to locating 13 critical trajectories. The effect of decreasing  $\alpha$  has not been analyzed but would lead to a finer outline of the critical trajectory stream tube and a more accurate calculation of  $A_o$ . One anomaly in the output was seen when the ray specified coincided with the corners of the inlet. Critical trajectories associated with these rays tended to lie outside range of critical trajectories on either side of this point. In one program test, eliminating these rays from the program improved the model result from a 26% to a 4% error.

The results presented in this paper show that the solutions agree with the unified empirical model of Hangal and Willeke (1990). The advantage of this model is that it can be expanded to situations beyond that investigated. These situations include modeling a yaw angle, multiple inlets, and inlets of different geometry. Modeling a yaw

angle as opposed to a pitch angle would require only a shift in the direction of the gravity component in the currently available boundary file. Modeling of multiple inlets and differing inlet geometries could be accomplished by reworking boundary files to represent the new inlet configurations.

## CONCLUSION

The boundary integral equation method can be used to accurately describe the air flow field into a thin edged inlet. Once the flow is described, Alenius's (1989) analytical solution to the particle equations of motion can be used to locate critical aerosol trajectories and accurately predict aspiration efficiency. A simple two dimensional model described here can accurately predict aspiration efficiency for small particles when the velocity ratio is close to 1. In this case, the critical trajectories are symmetric about the center of the inlet. When an angle of misalignment is introduced and/or the velocity ratios differ significantly from 1.0, a three dimensional model is required to describe critical trajectories and thus aspiration efficiency.

The 3D model can accurately predict aspiration efficiencies which are in good agreement with the unified aspiration efficiency model for all forward sampling angles proposed by Hangal and Willeke (1990). Further refinements to the model should improve the accuracy of aspiration efficiency estimates.

Finally, this model has the capability of predicting aspiration efficiencies for inlets of differing shapes and orientations including multiple inlets, yaw angles, and inlets of differing geometry. By reworking the boundary input files, inlets of any geometry, location, sampling angle and size can be studied using these programs.

## FUTURE WORK

Successful calculation of particle trajectories depends on several adjustable variables in the program including boundary discretization, calculation time step, convergence criteria, and capture criteria. While this paper demonstrates that the method can accurately track particles for given conditions, the above variable have not been tested to determine their optimum values. A study of these variables will help determine the contribution of each to the overall error in the program.

Boundary discretization of the 3D domain required to solve the BIEM problem can be difficult due to the number of triangular elements required. Also, when constructing a closed domain, a number of common nodes appear along the edges of each face of the boundary and at the corners. This can lead to cases where one node is contained in up to 6 distinct triangular elements. Boundary files for this project were manually prepared for about 50% of the domain. Full automation of this process would greatly increase the applicability of this method.

Finer discretization at the face of the inlet and along the walls of the inlet will decrease the distance a particle can come within the inlet and inlet sides before internal air velocity calculations no longer represent the conditions. In this project, that distance was 0.05 cm. This will lead to a significant increase in the number of

nodes and triangular elements required to describe the boundary and may increase the size of the boundary file by as much as 50% and subsequently increase computing time. Finer discretization may be avoided by adding an interpolation scheme to the program. This subroutine would be invoked when the particle entered the volume around the face of the inlet where internal velocity calculations showed large error. While this will cause some error in the prediction of internal velocity, it is expected it will be less than that of assuming a captured trajectory has occurred when the particle enters this area.

Rediscretization of the inlet and walls to more closely represent a circular inlet may also lead to a better comparison of the model with the unified aspiration efficiency equation. This could be done by modelling the inlet as an equal area hexagon or octagon. Automation of the boundary file would be paramount in this case as the discretization would become extremely tedious.

It may be necessary to add a routine to the program to automatically decrease the time step if the distance between successive points becomes large or the particle jumps across the boundaries of the inlet. Alternatively, the path of the particle can be analyzed to see if it crossed the inlet and a routine added to the capture criteria which records a capture when this situation occurs.

The boundary input files and start point routines were designed for positive sampling angles only. The program is

not general enough to support negative (downward pointing) inlet orientations. However, by simply changing the sign on the gravity vector and representing the negative angle as a positive angle, predictions of aspiration efficiency may be obtained.

Combination of the 3D boundary solution program with the particle tracking routine and the area integration routine would further streamline the efficiency calculations. Currently, 3 FORTRAN programs are used to calculate aspiration efficiency.



**APPENDIX**

### Calculation of Particle Trajectories:

Particle transport is influenced by a gravity force and a drag force due to the friction of the surrounding air. By Newton's second law, particle mass times acceleration is equal to the sum of the forces on the particle,

$$\sum \mathbf{F} = m\mathbf{a} \quad (1)$$

where  $\mathbf{F}$  is the force,  $\mathbf{a}$  is the acceleration and bold face quantities represent vectors.

The frictional force can be expressed by the following equation:

$$\mathbf{F}_d = - \frac{C_d(\text{Re})}{CC} \frac{A_p \rho_l \mathbf{v}_r \mathbf{v}_r}{2} \quad (2)$$

where

$C_d(\text{Re})$  is the dimensionless friction factor  
dependent on the Reynolds number

$CC$  is the Cunningham slip correction

$A_p$  is the projected area of the particle

$\rho_l$  is the density of the medium (air)

$\mathbf{v}_r$  is the magnitude of the particle relative  
velocity

$v_r$  is the particle velocity relative to the air.

$C_d(Re)$  is dependent on the particle Reynold's number,

$$Re = \frac{v_r dp \rho_l}{\mu_l} \quad (3)$$

where

$dp$  is the particle diameter (assumed spherical)

$\mu_l$  is the viscosity of the air.

Several expressions for  $C_d(Re)$  can be found in the literature (Reist, 1984) with most yielding no major deviation (Alenius, 1987). For this project the expressions used by Alenius are incorporated into a simplifying expression:

$$C_d(Re) = 24/Re \cdot Q(Re)$$

where  $Q(Re)$  is defined as: (4)

$$\begin{aligned} Q(Re) &= 1 && \text{for } 0 < Re \leq 0.5 \\ Q(Re) &= 1 + 0.15 Re^{0.687} && \text{for } 0.5 < Re \leq 800 \\ Q(Re) &= 0.44 Re/24 && \text{for } 800 < Re < 20000. \end{aligned}$$

By combining equations (3) and (4) into equation (2) and introducing the expression for particle relaxation time,  $\tau$ , a simplified expression for the drag force becomes:

$$Fd/m = Q(Re)/\tau \quad vr \quad (5)$$

where

$$\tau = \frac{dp^2 \, pl \, CC}{18 \, \mu l} \quad (6)$$

From equations (1) and (5) the particle motion can be described as:

$$d^2r/dt^2 - [Q(Re)/\tau(u-(dr/dt))]-g = 0 \quad (7)$$

where

$r$  is the particle position vector

$g$  is the acceleration due to gravity

$u$  is the air velocity at the point where the particle is located.

Equation (7) is analytically solvable if the factor  $Q(Re)$  is constant and the air velocity  $u$  at the points where the particle is successively located can be described as a linear function of the time that has elapsed until the particle reached the point. This condition can be approximately met if the motion is calculated in sufficiently small time steps.

If we introduce an expression for the linear behavior of the air velocity over the time interval being studied, then:

$$u(t) = (u(t)-u(t-t'))/t'+b \quad (8)$$

where

t is time  
t' is the length of the time step  
b is some initial value of velocity

For ease of writing we define the first part of the above expression as ua:

$$ua = (u(t)-u(t-t'))/t' \quad (9)$$

Now if we let  $A=Q(Re)/\tau$  equation (7) can be rewritten as:

$$dv/dt - A(ua+b) + Av - g = 0$$

recognizing that  $d^2r/dt^2 = dv/dt$ ,

$$\text{or,} \quad dv/dt + Av = A(ua+b) - g \quad (10)$$

If equation (10) is multiplied through by  $e^{\lambda t}$  the left hand side of the equation will be a derivative.

$$e^{\lambda t}(dv/dt) + e^{\lambda t}(Av) = (e^{\lambda t})A(ua+b) - g(e^{\lambda t})$$

Integrating both sides of the above equation from  $t_1$  to  $t_2$  gives:

$$\begin{aligned} v(t_2)e^{\lambda t_2} - v(t_1)e^{\lambda t_1} &= [(ua t_2)e^{\lambda t_2} - (ua/A)e^{\lambda t_2} \\ &\quad + (b)e^{\lambda t_2} + (g/A)e^{\lambda t_2}] \\ &\quad - [(ua t_2)e^{\lambda t_1} - (ua/A)e^{\lambda t_1} \\ &\quad + (b)e^{\lambda t_1} + (g/A)e^{\lambda t_1}] \end{aligned} \quad (11)$$

Adding  $v(t_1)e^{At_1}$  to both side of the equation, dividing through by  $e^{At_2}$  and simplifying gives an expression for  $v(t_2)$ :

$$v(t_2) = uat_2 - ua/A + b + g/A - \{(uat_1) - ua/A + b + g/A - v(t_1)\}e^{A(t_1-t_2)} \quad (12)$$

If we define a simplifying term,

$$u_b = u(t) - (u_a - g)\tau/Q(Re)$$

and define  $t_1$  as  $t$ , and  $t_2$  as the time at the end of the times step,  $t'$  ( $t_2 = t + t'$ ), substitute the air velocity at time  $t$  for  $b$ , and replace  $A$  with  $Q(Re)/\tau$ , then the solution is:

$$v(t+t') = u_at' + u_b - (u_b - v(t))\exp-[Q(Re)t'/\tau] \quad (13)$$

Integrating the equation (13) again will give the particle position:

$$r(t+t') = r(t) + u_at'/2 + u_bt' - (u_b - v(t))\tau/Q(Re)(1 - \exp Q(Re)t'/\tau) \quad (14)$$

Equation (13) and (14) are analytical solutions to the particle equations of motion and are used in both the 2D and 3D particle tracking subroutines.

# 2D Boundary Discretization Sample:

Potential specified on top and rear sides.  
Velocity specified over front, bottom, inlet face  
and sides.

DIN	1 cm	(inlet diameter)
THETA	30 degrees	(nozzle angle)
UI	1000 cm/sec	(sampling velocity)
UO	-250 cm/sec	(wind velocity)
UOX	-216.5064	(x component of UO)
UOY	125	(y component)

<u>NODE</u>	<u>X</u>	<u>Y</u>	<u>PHI</u>	<u>DPHI</u>	<u>ID</u>	<u>ICT</u>
1	20	15	0	-216.5064	3	0
2	20	10	0	-216.5064	3	0
3	20	5	0	-216.5064	3	0
4	20	0	0	-216.5064	3	0
5	20	-5	0	-216.5064	3	0
6	20	-10	0	-216.5064	3	0
7	20	-15	0	-216.5064	3	0
8	20	-20	0	-216.5064	3	0
9	19.99	-20	0	-125	3	0
10	15	-20	0	-125	3	0
11	10	-20	0	-125	3	0
12	5	-20	0	-125	3	0
13	0	-20	0	-125	3	0
14	-5	-20	0	-125	3	0
15	-10	-20	0	-125	3	0
16	-15	-20	0	-125	3	0
17	-20	-20	1830.13	0	2	1
18	-20	-15	2455.13	0	2	0
19	-20	-10	3080.13	0	2	0
20	-20	-5	3705.13	0	2	0
21	-20	-0.5	4267.63	0	2	2
22	-17.5	-0.5	0	0	3	0
23	-15	-0.5	0	0	3	0
24	-12.5	-0.5	0	0	3	0
25	-10	-0.5	0	0	3	0
26	-7.5	-0.5	0	0	3	0
27	-5	-0.5	0	0	3	0
28	-4.5	-0.5	0	0	3	0
29	-4	-0.5	0	0	3	0
30	-3.5	-0.5	0	0	3	0
31	-3	-0.5	0	0	3	0
32	-2.5	-0.5	0	0	3	0
33	-2	-0.5	0	0	3	0
34	-1.5	-0.5	0	0	3	0
35	-1	-0.5	0	0	3	0

36	-0.5	-0.5	0	0	3	0
37	0	-0.5	0	0	3	0
38	0	-0.499	0	1000	3	0
39	0	-0.375	0	1000	3	0
40	0	-0.25	0	1000	3	0
41	0	-0.125	0	1000	3	0
42	0	0	0	1000	3	0
43	0	0.125	0	1000	3	0
44	0	0.25	0	1000	3	0
45	0	0.375	0	1000	3	0
46	0	0.499	0	1000	3	0
47	0	0.5	0	0	3	0
48	-0.5	0.5	0	0	3	0
49	-1	0.5	0	0	3	0
50	-1.5	0.5	0	0	3	0
51	-2	0.5	0	0	3	0
52	-2.5	0.5	0	0	3	0
53	-3	0.5	0	0	3	0
54	-3.5	0.5	0	0	3	0
55	-4	0.5	0	0	3	0
56	-4.5	0.5	0	0	3	0
57	-5	0.5	0	0	3	0
58	-7.5	0.5	0	0	3	0
59	-10	0.5	0	0	3	0
60	-12.5	0.5	0	0	3	0
61	-15	0.5	0	0	3	0
62	-17.5	0.5	0	0	3	0
63	-20	0.5	4392.63	0	2	1
64	-20	5	4955.13	0	2	0
65	-20	10	5580.13	0	2	0
66	-20	15	6205.13	0	2	0
67	-20	20	6830.13	0	2	0
68	-15	20	5747.6	0	2	0
69	-10	20	4665.06	0	2	0
70	-5	20	3582.53	0	2	0
71	0	20	2500	0	2	0
72	5	20	1417.47	0	2	0
73	10	20	334.94	0	2	0
74	15	20	-747.6	0	2	0
75	20	20	0	-216.5064	3	2

3D Boundary Discretization Sample:

INPUT FILE FOR 3D CASE, 367 NODE, 693 ELEMENTS

Potential specified at all faces except at boudary of tube  
and at the face. ~~Four~~ corners specified with potential.

8

DIN	1 cm	(inlet diameter)
THETA	30 degrees	(nozzle angle)
UI	1000 cm/sec	(sampling velocity)
UO	-250 cm/sec	(wind velocity)
UOX	-216.5064	(x component of UO)
UOY	0	(y component)
UOZ	125	(z component)

NODE	X	Y	Z	PHI	DPHI	ID	ICT
1	0	-0.5	-0.5	0	0	2	0
2	0	-0.5	-0.499	0	0	2	0
3	0	-0.5	-0.375	0	0	2	0
4	0	-0.5	-0.25	0	0	2	0
5	0	-0.5	-0.125	0	0	2	0
6	0	-0.5	0	0	0	2	0
7	0	-0.5	0.125	0	0	2	0
8	0	-0.5	0.25	0	0	2	0
9	0	-0.5	0.375	0	0	2	0
10	0	-0.5	0.499	0	0	2	0
11	0	-0.5	0.5	0	0	2	0
12	0	-0.499	-0.5	0	0	2	0
13	0	-0.499	-0.499	0	1000	2	0
14	0	-0.499	-0.375	0	1000	2	0
15	0	-0.499	-0.25	0	1000	2	0
16	0	-0.499	-0.125	0	1000	2	0
17	0	-0.499	0	0	1000	2	0
18	0	-0.499	0.125	0	1000	2	0
19	0	-0.499	0.25	0	1000	2	0
20	0	-0.499	0.375	0	1000	2	0
21	0	-0.499	0.499	0	1000	2	0
22	0	-0.499	0.5	0	0	2	0
23	0	-0.375	-0.5	0	0	2	0
24	0	-0.375	-0.499	0	1000	2	0
25	0	-0.375	-0.375	0	1000	2	0
26	0	-0.375	-0.25	0	1000	2	0
27	0	-0.375	-0.125	0	1000	2	0
28	0	-0.375	0	0	1000	2	0
29	0	-0.375	0.125	0	1000	2	0
30	0	-0.375	0.25	0	1000	2	0
31	0	-0.375	0.375	0	1000	2	0
32	0	-0.375	0.499	0	1000	2	0
33	0	-0.375	0.5	0	0	2	0
34	0	-0.25	-0.5	0	0	2	0
35	0	-0.25	-0.499	0	1000	2	0
36	0	-0.25	-0.375	0	1000	2	0
37	0	-0.25	-0.25	0	1000	2	0
38	0	-0.25	-0.125	0	1000	2	0
39	0	-0.25	0	0	1000	2	0
40	0	-0.25	0.125	0	1000	2	0
41	0	-0.25	0.25	0	1000	2	0
42	0	-0.25	0.375	0	1000	2	0
43	0	-0.25	0.499	0	1000	2	0
44	0	-0.25	0.5	0	0	2	0
45	0	-0.125	-0.5	0	0	2	0
46	0	-0.125	-0.499	0	1000	2	0
47	0	-0.125	-0.375	0	1000	2	0
48	0	-0.125	-0.25	0	1000	2	0
49	0	-0.125	-0.125	0	1000	2	0
50	0	-0.125	0	0	1000	2	0
51	0	-0.125	0.125	0	1000	2	0
52	0	-0.125	0.25	0	1000	2	0
53	0	-0.125	0.375	0	1000	2	0

54	0	-0.125	0.499	0	1000	2	0
55	0	-0.125	0.5	0	0	2	0
56	0	0	-0.5	0	0	2	0
57	0	0	-0.499	0	1000	2	0
58	0	0	-0.375	0	1000	2	0
59	0	0	-0.25	0	1000	2	0
60	0	0	-0.125	0	1000	2	0
61	0	0	0	0	1000	2	0
62	0	0	0.125	0	1000	2	0
63	0	0	0.25	0	1000	2	0
64	0	0	0.375	0	1000	2	0
65	0	0	0.499	0	1000	2	0
66	0	0	0.5	0	0	2	0
67	0	0.125	-0.5	0	0	2	0
68	0	0.125	-0.499	0	1000	2	0
69	0	0.125	-0.375	0	1000	2	0
70	0	0.125	-0.25	0	1000	2	0
71	0	0.125	-0.125	0	1000	2	0
72	0	0.125	0	0	1000	2	0
73	0	0.125	0.125	0	1000	2	0
74	0	0.125	0.25	0	1000	2	0
75	0	0.125	0.375	0	1000	2	0
76	0	0.125	0.499	0	1000	2	0
77	0	0.125	0.5	0	0	2	0
78	0	0.25	-0.5	0	0	2	0
79	0	0.25	-0.499	0	1000	2	0
80	0	0.25	-0.375	0	1000	2	0
81	0	0.25	-0.25	0	1000	2	0
82	0	0.25	-0.125	0	1000	2	0
83	0	0.25	0	0	1000	2	0
84	0	0.25	0.125	0	1000	2	0
85	0	0.25	0.25	0	1000	2	0
86	0	0.25	0.375	0	1000	2	0
87	0	0.25	0.499	0	1000	2	0
88	0	0.25	0.5	0	0	2	0
89	0	0.375	-0.5	0	0	2	0
90	0	0.375	-0.499	0	1000	2	0
91	0	0.375	-0.375	0	1000	2	0
92	0	0.375	-0.25	0	1000	2	0
93	0	0.375	-0.125	0	1000	2	0
94	0	0.375	0	0	1000	2	0
95	0	0.375	0.125	0	1000	2	0
96	0	0.375	0.25	0	1000	2	0
97	0	0.375	0.375	0	1000	2	0
98	0	0.375	0.499	0	1000	2	0
99	0	0.375	0.5	0	0	2	0
100	0	0.499	-0.5	0	0	2	0
101	0	0.499	-0.499	0	1000	2	0
102	0	0.499	-0.375	0	1000	2	0
103	0	0.499	-0.25	0	1000	2	0
104	0	0.499	-0.125	0	1000	2	0
105	0	0.499	0	0	1000	2	0
106	0	0.499	0.125	0	1000	2	0
107	0	0.499	0.25	0	1000	2	0

108	0	0.499	0.375	0	1000	2	0
109	0	0.499	0.499	0	1000	2	0
110	0	0.499	0.5	0	0	2	0
111	0	0.5	-0.5	0	0	2	0
112	0	0.5	-0.499	0	0	2	0
113	0	0.5	-0.375	0	0	2	0
114	0	0.5	-0.25	0	0	2	0
115	0	0.5	-0.125	0	0	2	0
116	0	0.5	0	0	0	2	0
117	0	0.5	0.125	0	0	2	0
118	0	0.5	0.25	0	0	2	0
119	0	0.5	0.375	0	0	2	0
120	0	0.5	0.499	0	0	2	0
121	0	0.5	0.5	0	0	2	0
122	-0.5	-0.5	-0.5	0	0	2	0
123	-1	-0.5	-0.5	0	0	2	0
124	-1.5	-0.5	-0.5	0	0	2	0
125	-2	-0.5	-0.5	0	0	2	0
126	-2.5	-0.5	-0.5	0	0	2	0
127	-3	-0.5	-0.5	0	0	2	0
128	-3.5	-0.5	-0.5	0	0	2	0
129	-4	-0.5	-0.5	0	0	2	0
130	-4.5	-0.5	-0.5	0	0	2	0
131	-5	-0.5	-0.5	0	0	2	0
132	-0.5	0	-0.5	0	0	2	0
133	-1	0	-0.5	0	0	2	0
134	-1.5	0	-0.5	0	0	2	0
135	-2	0	-0.5	0	0	2	0
136	-2.5	0	-0.5	0	0	2	0
137	-3	0	-0.5	0	0	2	0
138	-3.5	0	-0.5	0	0	2	0
139	-4	0	-0.5	0	0	2	0
140	-4.5	0	-0.5	0	0	2	0
141	-5	0	-0.5	0	0	2	0
142	-0.5	0.5	-0.5	0	0	2	0
143	-1	0.5	-0.5	0	0	2	0
144	-1.5	0.5	-0.5	0	0	2	0
145	-2	0.5	-0.5	0	0	2	0
146	-2.5	0.5	-0.5	0	0	2	0
147	-3	0.5	-0.5	0	0	2	0
148	-3.5	0.5	-0.5	0	0	2	0
149	-4	0.5	-0.5	0	0	2	0
150	-4.5	0.5	-0.5	0	0	2	0
151	-5	0.5	-0.5	0	0	2	0
152	-0.5	0.5	0	0	0	2	0
153	-1	0.5	0	0	0	2	0
154	-1.5	0.5	0	0	0	2	0
155	-2	0.5	0	0	0	2	0
156	-2.5	0.5	0	0	0	2	0
157	-3	0.5	0	0	0	2	0
158	-3.5	0.5	0	0	0	2	0
159	-4	0.5	0	0	0	2	0
160	-4.5	0.5	0	0	0	2	0
161	-5	0.5	0	0	0	2	0

162	-0.5	0.5	0.5	0	0	2	0
163	-1	0.5	0.5	0	0	2	0
164	-1.5	0.5	0.5	0	0	2	0
165	-2	0.5	0.5	0	0	2	0
166	-2.5	0.5	0.5	0	0	2	0
167	-3	0.5	0.5	0	0	2	0
168	-3.5	0.5	0.5	0	0	2	0
169	-4	0.5	0.5	0	0	2	0
170	-4.5	0.5	0.5	0	0	2	0
171	-5	0.5	0.5	0	0	2	0
172	-0.5	0	0.5	0	0	2	0
173	-1	0	0.5	0	0	2	0
174	-1.5	0	0.5	0	0	2	0
175	-2	0	0.5	0	0	2	0
176	-2.5	0	0.5	0	0	2	0
177	-3	0	0.5	0	0	2	0
178	-3.5	0	0.5	0	0	2	0
179	-4	0	0.5	0	0	2	0
180	-4.5	0	0.5	0	0	2	0
181	-5	0	0.5	0	0	2	0
182	-0.5	-0.5	0.5	0	0	2	0
183	-1	-0.5	0.5	0	0	2	0
184	-1.5	-0.5	0.5	0	0	2	0
185	-2	-0.5	0.5	0	0	2	0
186	-2.5	-0.5	0.5	0	0	2	0
187	-3	-0.5	0.5	0	0	2	0
188	-3.5	-0.5	0.5	0	0	2	0
189	-4	-0.5	0.5	0	0	2	0
190	-4.5	-0.5	0.5	0	0	2	0
191	-5	-0.5	0.5	0	0	2	0
192	-0.5	-0.5	0	0	0	2	0
193	-1	-0.5	0	0	0	2	0
194	-1.5	-0.5	0	0	0	2	0
195	-2	-0.5	0	0	0	2	0
196	-2.5	-0.5	0	0	0	2	0
197	-3	-0.5	0	0	0	2	0
198	-3.5	-0.5	0	0	0	2	0
199	-4	-0.5	0	0	0	2	0
200	-4.5	-0.5	0	0	0	2	0
201	-5	-0.5	0	0	0	2	0
202	-7.5	-0.5	-0.5	0	0	2	0
203	-10	-0.5	-0.5	0	0	2	0
204	-12.5	-0.5	-0.5	0	0	2	0
205	-15	-0.5	-0.5	0	0	2	0
206	-17.5	-0.5	-0.5	0	0	2	0
207	-20	-0.5	-0.5	4268	0	1	1
208	-7.5	0.5	-0.5	0	0	2	0
209	-10	0.5	-0.5	0	0	2	0
210	-12.5	0.5	-0.5	0	0	2	0
211	-15	0.5	-0.5	0	0	2	0
212	-17.5	0.5	-0.5	0	0	2	0
213	-20	0.5	-0.5	4268	0	1	1
214	-7.5	0.5	0.5	0	0	2	0
215	-10	0.5	0.5	0	0	2	0

216	-12.5	0.5	0.5	0	0	2	0
217	-15	0.5	0.5	0	0	2	0
218	-17.5	0.5	0.5	0	0	2	0
219	-20	0.5	0.5	4393	0	1	1
220	-7.5	-0.5	0.5	0	0	2	0
221	-10	-0.5	0.5	0	0	2	0
222	-12.5	-0.5	0.5	0	0	2	0
223	-15	-0.5	0.5	0	0	2	0
224	-17.5	-0.5	0.5	0	0	2	0
225	-20	-0.5	0.5	4393	0	1	1
226	-20	-20	-20	1830	0	1	0
227	-20	-20	-10	3080	0	1	0
228	-20	-20	0	4330	0	1	0
229	-20	-20	10	5580	0	1	0
230	-20	-20	20	6830	0	1	0
231	-20	-10	-20	1830	0	1	0
232	-20	-10	-10	3080	0	1	0
233	-20	-10	0	4330	0	1	0
234	-20	-10	10	5580	0	1	0
235	-20	-10	20	6830	0	1	0
236	-20	0	-20	1830	0	1	0
237	-20	-0.501	0.501	4393	0	1	0
238	-20	-0.501	0	4330	0	1	0
239	-20	0.501	-0.501	4268	0	1	0
240	-20	0	10	5580	0	1	0
241	-20	0	20	6830	0	1	0
242	-20	0	-10	3080	0	1	0
243	-20	0.501	0.501	4393	0	1	0
244	-20	0.501	0	4330	0	1	0
245	-20	-0.501	-0.501	4268	0	1	0
246	-20	10	-20	1830	0	1	0
247	-20	10	-10	3080	0	1	0
248	-20	10	0	4330	0	1	0
249	-20	10	10	5580	0	1	0
250	-20	10	20	6830	0	1	0
251	-20	20	-20	1830	0	1	0
252	-20	20	-10	3080	0	1	0
253	-20	20	0	4330	0	1	0
254	-20	20	10	5580	0	1	0
255	-20	20	20	6830	0	1	0
256	20	-20	20	-1830	0	1	0
257	10	-20	20	334.9	0	1	0
258	0	-20	20	2500	0	1	0
259	-10	-20	20	4665	0	1	0
260	20	-20	10	-3080	0	1	0
261	10	-20	10	-915	0	1	0
262	0	-20	10	1250	0	1	0
263	-10	-20	10	3415	0	1	0
264	20	-20	0	-4330	0	1	0
265	10	-20	0	-2165	0	1	0
266	0	-20	0	0	0	1	0
267	-10	-20	0	2165	0	1	0
268	20	-20	-10	-5580	0	1	0
269	10	-20	-10	-3415	0	1	0

270	0	-20	-10	-1250	0	1	0
271	-10	-20	-10	915.1	0	1	0
272	20	-20	-20	-6830	0	1	0
273	10	-20	-20	-4665	0	1	0
274	0	-20	-20	-2500	0	1	0
275	-10	-20	-20	-335	0	1	0
276	20	-10	20	-1830	0	1	0
277	20	-10	10	-3080	0	1	0
278	20	-10	0	-4330	0	1	0
279	20	-10	-10	-5580	0	1	0
280	20	-10	-20	-6830	0	1	0
281	20	0	20	-1830	0	1	0
282	20	0	10	-3080	0	1	0
283	20	0	0	-4330	0	1	0
284	20	0	-10	-5580	0	1	0
285	20	0	-20	-6830	0	1	0
286	20	10	20	-1830	0	1	0
287	20	10	10	-3080	0	1	0
288	20	10	0	-4330	0	1	0
289	20	10	-10	-5580	0	1	0
290	20	10	-20	-6830	0	1	0
291	20	20	20	-1830	0	1	0
292	20	20	10	-3080	0	1	0
293	20	20	0	-4330	0	1	0
294	20	20	-10	-5580	0	1	0
295	20	20	-20	-6830	0	1	0
296	10	-10	-20	-4665	0	1	0
297	0	-10	-20	-2500	0	1	0
298	-10	-10	-20	-335	0	1	0
299	10	0	-20	-4665	0	1	0
300	0	0	-20	-2500	0	1	0
301	-10	0	-20	-335	0	1	0
302	10	10	-20	-4665	0	1	0
303	0	10	-20	-2500	0	1	0
304	-10	10	-20	-335	0	1	0
305	10	20	-20	-4665	0	1	0
306	0	20	-20	-2500	0	1	0
307	-10	20	-20	-335	0	1	0
308	0	-20	-20	-2500	0	1	0
309	19.999	-10	-20	-6830	0	1	0
310	19.999	0	-20	-6830	0	1	0
311	19.999	10	-20	-6830	0	1	0
312	19.999	20	-20	-6830	0	1	0
313	10	20	-10	-3415	0	1	0
314	0	20	-10	-1250	0	1	0
315	-10	20	-10	915.1	0	1	0
316	10	20	0	-2165	0	1	0
317	0	20	0	0	0	1	0
318	-10	20	0	2165	0	1	0
319	10	20	10	-915	0	1	0
320	0	20	10	1250	0	1	0
321	-10	20	10	3415	0	1	0
322	10	20	20	334.9	0	1	0
323	0	20	20	2500	0	1	0

324	-10	20	20	4665	0	1	0
325	10	10	20	334.9	0	1	0
326	0	10	20	2500	0	1	0
327	-10	10	20	4665	0	1	0
328	10	0	20	334.9	0	1	0
329	0	0	20	2500	0	1	0
330	-10	0	20	4665	0	1	0
331	10	-10	20	334.9	0	1	0
332	0	-10	20	2500	0	1	0
333	-10	-10	20	4665	0	1	0
334	20	-19.999	19.999	-1830	0	1	0
335	20	-19.999	10	-3080	0	1	0
336	20	-19.999	0	-4330	0	1	0
337	20	-19.999	-10	-5580	0	1	0
338	20	-19.999	-19.999	-6830	0	1	0
339	20	-10	-19.999	-6830	0	1	0
340	20	0	-19.999	-6830	0	1	0
341	20	10	-19.999	-6830	0	1	0
342	20	19.999	-19.999	-6830	0	1	0
343	20	19.999	-10	-5580	0	1	0
344	20	19.999	0	-4330	0	1	0
345	20	19.999	10	-3080	0	1	0
346	20	19.999	19.999	-1830	0	1	0
347	20	10	19.999	-1830	0	1	0
348	20	0	19.999	-1830	0	1	0
349	20	-10	19.999	-1830	0	1	0
350	-20	0	0.501	4393	0	1	0
351	-20	0	-0.501	4268	0	1	0
352	-20	-19.999	-19.999	1830	0	1	0
353	-20	-19.999	-10	3080	0	1	0
354	-20	-19.999	0	4330	0	1	0
355	-20	-19.999	10	5580	0	1	0
356	-20	-19.999	19.999	6830	0	1	0
357	-20	-10	-19.999	1830	0	1	0
358	-20	-10	19.999	6830	0	1	0
359	-20	0	-19.999	1830	0	1	0
360	-20	0	19.999	6830	0	1	0
361	-20	10	-19.999	1830	0	1	0
362	-20	10	19.999	6830	0	1	0
363	-20	19.999	-19.999	1830	0	1	0
364	-20	19.999	-10	3080	0	1	0
365	-20	19.999	0	4330	0	1	0
366	-20	19.999	10	5580	0	1	0
367	-20	19.999	19.999	6830	0	1	0

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
1	1	2	13	13
2	2	3	13	13
3	3	4	14	14
4	4	5	15	15
5	5	6	16	16
6	6	7	17	17
7	7	8	18	18
8	8	9	19	19
9	9	10	20	20
10	10	11	21	21
11	1	13	12	13
12	3	14	13	13
13	4	15	14	14
14	5	16	15	15
15	6	17	16	16
16	7	18	17	17
17	8	19	18	18
18	9	20	19	19
19	10	21	20	20
20	11	22	21	21
21	12	13	23	13
22	13	14	24	24
23	14	15	25	25
24	15	16	26	26
25	16	17	27	27
26	17	18	28	28
27	18	19	29	29
28	19	20	30	30
29	20	21	31	31
30	21	22	32	32
31	13	24	23	24
32	14	25	24	24
33	15	26	25	25
34	16	27	26	26
35	17	28	27	27
36	18	29	28	28
37	19	30	29	29
38	20	31	30	30
39	21	32	31	31
40	22	33	32	32
41	23	24	34	24
42	24	25	35	35
43	25	26	36	36
44	26	27	37	37
45	27	28	38	38
46	28	29	39	39
47	29	30	40	40
48	30	31	41	41
49	31	32	42	42
50	32	33	43	43
51	24	35	34	35
52	25	36	35	35
53	26	37	36	36

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
54	27	38	37	37
55	28	39	38	38
56	29	40	39	39
57	30	41	40	40
58	31	42	41	41
59	32	43	42	42
60	33	44	43	43
61	34	35	45	35
62	35	36	46	46
63	36	37	47	47
64	37	38	48	48
65	38	39	49	49
66	39	40	50	50
67	40	41	51	51
68	41	42	52	52
69	42	43	53	53
70	43	44	54	54
71	35	46	45	46
72	36	47	46	46
73	37	48	47	47
74	38	49	48	48
75	39	50	49	49
76	40	51	50	50
77	41	52	51	51
78	42	53	52	52
79	43	54	53	53
80	44	55	54	54
81	45	46	56	46
82	46	47	57	57
83	47	48	58	58
84	48	49	59	59
85	49	50	60	60
86	50	51	61	61
87	51	52	62	62
88	52	53	63	63
89	53	54	64	64
90	54	55	65	65
91	46	57	56	57
92	47	58	57	57
93	48	59	58	58
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96	51	62	61	61
97	52	63	62	62
98	53	64	63	63
99	54	65	64	64
100	55	66	65	65
101	56	57	67	57
102	57	58	68	68
103	58	59	69	69
104	59	60	70	70
105	60	61	71	71
106	61	62	72	72

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
107	62	63	73	73
108	63	64	74	74
109	64	65	75	75
110	65	66	76	76
111	57	68	67	68
112	58	69	68	68
113	59	70	69	69
114	60	71	70	70
115	61	72	71	71
116	62	73	72	72
117	63	74	73	73
118	64	75	74	74
119	65	76	75	75
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121	67	68	78	68
122	68	69	79	79
123	69	70	80	80
124	70	71	81	81
125	71	72	82	82
126	72	73	83	83
127	73	74	84	84
128	74	75	85	85
129	75	76	86	86
130	76	77	87	87
131	68	79	78	79
132	69	80	79	79
133	70	81	80	80
134	71	82	81	81
135	72	83	82	82
136	73	84	83	83
137	74	85	84	84
138	75	86	85	85
139	76	87	86	86
140	77	88	87	87
141	78	79	89	79
142	79	80	90	90
143	80	81	91	91
144	81	82	92	92
145	82	83	93	93
146	83	84	94	94
147	84	85	95	95
148	85	86	96	96
149	86	87	97	97
150	87	88	98	98
151	79	90	89	90
152	80	91	90	90
153	81	92	91	91
154	82	93	92	92
155	83	94	93	93
156	84	95	94	94
157	85	96	95	95
158	86	97	96	96
159	87	98	97	97

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
160	88	99	98	98
161	89	90	100	90
162	90	91	101	101
163	91	92	102	102
164	92	93	103	103
165	93	94	104	104
166	94	95	105	105
167	95	96	106	106
168	96	97	107	107
169	97	98	108	108
170	98	99	109	109
171	90	101	100	101
172	91	102	101	101
173	92	103	102	102
174	93	104	103	103
175	94	105	104	104
176	95	106	105	105
177	96	107	106	106
178	97	108	107	107
179	98	109	108	108
180	99	110	109	109
181	100	101	111	101
182	101	102	112	102
183	102	103	113	103
184	103	104	114	104
185	104	105	115	105
186	105	106	116	106
187	106	107	117	107
188	107	108	118	108
189	108	109	119	109
190	109	121	120	109
191	101	112	111	101
192	102	113	112	102
193	103	114	113	103
194	104	115	114	104
195	105	116	115	105
196	106	117	116	106
197	107	118	117	107
198	108	119	118	108
199	109	120	119	109
200	109	110	121	109
201	122	1	56	56
202	123	122	132	132
203	124	123	133	133
204	125	124	134	134
205	126	125	135	135
206	127	126	136	136
207	128	127	137	137
208	129	128	138	138
209	130	129	139	139
210	131	130	140	140
211	132	122	56	56
212	133	123	132	132

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
213	134	124	133	133
214	135	125	134	134
215	136	126	135	135
216	137	127	136	136
217	138	128	137	137
218	139	129	138	138
219	140	130	139	139
220	141	131	140	140
221	132	56	111	111
222	133	132	142	142
223	134	133	143	143
224	135	134	144	144
225	136	135	145	145
226	137	136	146	146
227	138	137	147	147
228	139	138	148	148
229	140	139	149	149
230	141	140	150	150
231	142	132	111	111
232	143	133	142	142
233	144	134	143	143
234	145	135	144	144
235	146	136	145	145
236	147	137	146	146
237	148	138	147	147
238	149	139	148	148
239	150	140	149	149
240	151	141	150	150
241	142	111	116	116
242	143	142	152	152
243	144	143	153	153
244	145	144	154	154
245	146	145	155	155
246	147	146	156	156
247	148	147	157	157
248	149	148	158	158
249	150	149	159	159
250	151	150	160	160
251	152	142	116	116
252	153	143	152	152
253	154	144	153	153
254	155	145	154	154
255	156	146	155	155
256	157	147	156	156
257	158	148	157	157
258	159	149	158	158
259	160	150	159	159
260	161	151	160	160
261	152	116	121	121
262	153	152	162	162
263	154	153	163	163
264	155	154	164	164
265	156	155	165	165

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
266	157	156	166	166
267	158	157	167	167
268	159	158	168	168
269	160	159	169	169
270	161	160	170	170
271	162	152	121	121
272	163	153	162	162
273	164	154	163	163
274	165	155	164	164
275	166	156	165	165
276	167	157	166	166
277	168	158	167	167
278	169	159	168	168
279	170	160	169	169
280	171	161	170	170
281	162	121	66	66
282	163	162	172	172
283	164	163	173	173
284	165	164	174	174
285	166	165	175	175
286	167	166	176	176
287	168	167	177	177
288	169	168	178	178
289	170	169	179	179
290	171	170	180	180
291	172	162	66	66
292	173	163	172	172
293	174	164	173	173
294	175	165	174	174
295	176	166	175	175
296	177	167	176	176
297	178	168	177	177
298	179	169	178	178
299	180	170	179	179
300	181	171	180	180
301	172	66	11	11
302	173	172	182	182
303	174	173	183	183
304	175	174	184	184
305	176	175	185	185
306	177	176	186	186
307	178	177	187	187
308	179	178	188	188
309	180	179	189	189
310	181	180	190	190
311	182	172	11	11
312	183	173	182	182
313	184	174	183	183
314	185	175	184	184
315	186	176	185	185
316	187	177	186	186
317	188	178	187	187
318	189	179	188	188

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
319	190	180	189	189
320	191	181	190	190
321	182	11	6	6
322	183	182	192	192
323	184	183	193	193
324	185	184	194	194
325	186	185	195	195
326	187	186	196	196
327	188	187	197	197
328	189	188	198	198
329	190	189	199	199
330	191	190	200	200
331	192	182	6	6
332	193	183	192	192
333	194	184	193	193
334	195	185	194	194
335	196	186	195	195
336	197	187	196	196
337	198	188	197	197
338	199	189	198	198
339	200	190	199	199
340	201	191	200	200
341	192	6	1	1
342	193	192	122	122
343	194	193	123	123
344	195	194	124	124
345	196	195	125	125
346	197	196	126	126
347	198	197	127	127
348	199	198	128	128
349	200	199	129	129
350	201	200	130	130
351	122	192	1	1
352	123	193	122	122
353	124	194	123	123
354	125	195	124	124
355	126	196	125	125
356	127	197	126	126
357	128	198	127	127
358	129	199	128	128
359	130	200	129	129
360	131	201	130	130
361	202	131	151	151
362	203	202	208	208
363	204	203	209	209
364	205	204	210	210
365	206	205	211	211
366	207	206	212	212
367	208	202	151	151
368	209	203	208	208
369	210	204	209	209
370	211	205	210	210
371	212	206	211	211

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
372	213	207	212	212
373	208	151	171	171
374	209	208	214	214
375	210	209	214	214
376	211	210	216	216
377	212	211	217	217
378	213	212	218	218
379	214	208	171	171
380	215	209	214	214
381	216	210	215	215
382	217	211	216	216
383	218	212	217	217
384	219	213	218	218
385	214	171	191	191
386	215	214	220	220
387	216	215	221	221
388	217	216	222	222
389	218	217	223	223
390	219	218	224	224
391	220	214	191	191
392	221	215	220	220
393	222	216	221	221
394	223	217	222	222
395	224	218	223	223
396	225	219	224	224
397	220	191	131	131
398	221	220	202	202
399	222	221	203	203
400	223	222	204	204
401	224	223	205	205
402	225	224	206	206
403	202	220	131	131
404	203	221	202	202
405	204	222	203	203
406	205	223	204	204
407	206	224	205	205
408	207	225	206	206
409	352	353	357	357
410	353	354	232	232
411	354	355	233	233
412	355	356	234	234
413	353	232	357	232
414	354	233	232	232
415	355	234	233	233
416	356	358	234	234
417	357	232	359	359
418	232	245	242	242
419	233	237	238	233
420	234	358	240	240
421	232	242	359	242
422	232	233	245	233
423	233	234	237	233
424	358	360	240	240

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
425	242	351	239	242
426	234	240	237	237
427	242	239	247	247
428	350	240	243	240
429	359	242	361	242
430	239	248	247	247
431	243	249	248	248
432	240	360	249	249
433	242	247	361	246
434	244	243	248	248
435	243	240	249	249
436	360	362	249	249
437	361	247	363	247
438	247	248	364	248
439	248	249	365	248
440	249	362	366	249
441	247	364	363	247
442	248	365	364	248
443	249	366	365	249
444	362	367	366	366
445	256	257	260	260
446	257	258	261	261
447	258	259	262	262
448	259	230	263	263
449	257	261	260	260
450	258	262	261	261
451	259	263	262	262
452	230	229	263	263
453	260	261	264	264
454	261	262	265	265
455	262	263	266	266
456	263	229	267	267
457	261	265	264	264
458	262	266	265	265
459	263	267	266	266
460	229	228	267	267
461	264	265	268	268
462	265	266	269	269
463	266	267	270	270
464	267	228	271	271
465	265	269	268	268
466	266	270	269	269
467	267	271	270	270
468	228	227	271	271
469	268	269	272	269
470	269	270	273	273
471	270	271	274	274
472	271	227	275	275
473	269	273	272	269
474	270	274	273	273
475	271	275	274	274
476	227	226	275	275
477	334	335	349	349

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
478	335	336	277	277
479	336	337	278	278
480	337	338	279	279
481	349	335	277	277
482	336	278	277	277
483	337	279	278	278
484	338	339	279	279
485	348	349	277	277
486	277	278	282	282
487	278	279	283	283
488	279	339	284	284
489	277	282	348	282
490	278	283	282	282
491	279	284	283	283
492	339	340	284	284
493	347	348	282	282
494	282	283	287	287
495	283	284	288	288
496	284	340	289	289
497	282	287	347	287
498	283	288	287	287
499	284	289	288	288
500	340	341	289	289
501	347	287	346	287
502	287	288	345	288
503	344	288	289	289
504	341	343	289	289
505	345	346	287	287
506	344	345	288	288
507	343	344	289	289
508	341	342	343	343
509	308	273	309	308
510	273	274	296	296
511	274	275	297	297
512	275	226	298	298
513	273	296	309	309
514	274	297	296	296
515	275	298	297	297
516	226	231	298	298
517	309	296	310	310
518	296	297	299	299
519	297	298	300	300
520	298	231	301	301
521	296	299	310	310
522	297	300	299	299
523	298	301	300	300
524	231	236	301	301
525	310	299	311	311
526	299	300	302	302
527	300	301	303	303
528	301	236	304	304
529	299	302	311	311
530	300	303	302	302

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
531	301	304	303	303
532	236	246	304	304
533	311	302	312	312
534	302	303	305	305
535	303	304	306	306
536	304	246	307	307
537	302	305	312	312
538	303	306	305	305
539	304	307	306	306
540	246	251	307	307
541	272	308	280	308
542	308	309	280	309
543	280	309	285	309
544	309	310	285	309
545	285	310	290	310
546	310	311	290	310
547	290	311	295	311
548	311	312	295	311
549	295	305	294	305
550	305	306	313	313
551	306	307	314	314
552	307	251	315	315
553	305	313	294	313
554	306	314	313	314
555	307	315	314	315
556	251	252	315	315
557	294	313	293	313
558	313	314	316	316
559	314	315	317	317
560	315	252	318	318
561	313	316	293	316
562	314	317	316	316
563	315	318	317	317
564	252	253	318	318
565	293	316	292	316
566	316	317	319	319
567	317	318	320	320
568	318	253	321	321
569	316	319	292	319
570	317	320	319	319
571	318	321	320	320
572	253	254	321	321
573	292	319	291	319
574	319	320	322	322
575	320	321	323	323
576	321	254	324	324
577	319	322	291	322
578	320	323	322	322
579	321	324	323	323
580	254	255	324	324
581	291	322	286	322
582	322	323	325	325
583	323	324	326	326

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
584	324	255	327	327
585	322	325	286	322
586	323	326	325	325
587	324	327	326	326
588	255	250	327	327
589	286	325	281	325
590	325	326	328	328
591	326	327	329	329
592	327	250	330	330
593	325	328	281	325
594	326	329	328	328
595	327	330	329	329
596	250	241	330	330
597	281	328	276	328
598	328	329	331	331
599	329	330	332	332
600	330	241	333	333
601	328	331	276	328
602	329	332	331	331
603	330	333	332	332
604	241	235	333	333
605	276	331	256	331
606	331	332	257	257
607	332	333	258	258
608	333	235	259	259
609	331	257	256	256
610	332	258	257	257
611	333	259	258	258
612	235	230	259	259
613	256	335	334	334
614	260	264	335	335
615	264	268	336	336
616	268	272	337	337
617	349	256	334	334
618	256	260	335	335
619	264	336	335	335
620	268	337	336	336
621	272	338	337	337
622	276	256	349	349
623	338	272	339	339
624	272	280	339	339
625	281	276	349	349
626	281	349	348	348
627	339	280	340	340
628	280	285	340	340
629	286	281	348	348
630	286	348	347	347
631	340	285	341	341
632	285	290	341	341
633	291	286	347	347
634	291	347	346	346
635	295	342	341	341
636	290	295	341	341

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
637	291	346	345	345
638	292	291	345	345
639	344	292	345	345
640	293	292	344	344
641	293	344	343	343
642	294	293	343	343
643	295	294	343	343
644	295	343	342	342
645	226	353	352	352
646	226	227	353	353
647	227	228	353	353
648	228	354	353	353
649	228	229	354	354
650	229	355	354	354
651	229	230	355	355
652	230	356	355	355
653	231	226	357	357
654	226	352	357	357
655	356	230	358	358
656	230	235	358	358
657	236	231	357	357
658	236	357	359	359
659	358	235	360	360
660	235	241	360	360
661	246	236	359	359
662	246	359	361	361
663	360	241	362	362
664	241	250	362	362
665	251	246	361	361
666	251	361	363	363
667	255	367	362	362
668	250	255	362	362
669	251	363	364	364
670	252	251	364	364
671	252	364	365	365
672	253	252	365	365
673	366	253	365	365
674	254	253	366	366
675	255	254	366	366
676	255	366	367	367
677	207	245	238	238
678	225	207	238	238
679	225	238	237	237
680	225	237	350	350
681	219	225	350	350
682	219	350	243	243
683	219	243	244	244
684	213	219	244	244
685	213	244	239	239
686	351	213	239	239
687	207	213	351	351
688	350	237	240	240
689	245	351	242	242

<u>ELEM</u>	<u>NODE1</u>	<u>NODE2</u>	<u>NODE3</u>	<u>NODE4</u>
690	272	269	308	269
691	295	312	294	312
692	239	244	248	248
693	245	233	238	233

# Two Dimensional Model Output

Time Step = 0.003 seconds

Convergence Criteria = 0.001

<u>U0,cm/sec</u>	<u>Ui,cm/sec</u>	<u>Theta</u>	<u>d, um</u>	<u>D, cm</u>	MODEL <u>Eff.</u>	UNIFIED <u>MODEL EFF</u>
250	125	0	5	1.00	1.17	1.0420
250	125	0	40	1.00	1.71	1.7372
500	125	0	5	1.00	1.55	1.2268
500	125	0	40	1.00	3.40	3.5187
1000	125	0	5	1.00	2.39	1.9534
1000	125	0	40	1.00	7.04	7.3689
250	250	0	5	1.00	0.99	1.0000
250	250	0	40	1.00	1.00	1.0000
500	250	0	5	1.00	1.20	1.0806
500	250	0	40	1.00	1.81	1.8487
1000	250	0	5	1.00	1.69	1.4217
1000	250	0	40	1.00	3.58	3.7384
250	500	0	5	1.00	0.89	0.9710
250	500	0	40	1.00	0.64	0.6013
500	500	0	5	1.00	0.99	1.0000
500	500	0	40	1.00	1.00	1.0000
1000	500	0	5	1.00	1.26	1.1492
1000	500	0	40	1.00	1.87	1.9182
250	1000	0	5	1.00	0.82	0.9412
250	1000	0	40	1.00	0.46	0.3665
500	1000	0	5	1.00	0.86	0.9453
500	1000	0	40	1.00	0.60	0.5564
1000	1000	0	5	1.00	0.99	1.0000
1000	1000	0	40	1.00	1.00	1.0000
250	125	0	5	0.32	1.25	1.1205
250	125	0	40	0.32	1.83	1.8976
500	125	0	5	0.32	1.83	1.6106
500	125	0	40	0.32	3.72	3.8271
1000	125	0	5	0.32	3.41	3.3106
1000	125	0	40	0.32	7.64	7.7848
250	250	0	5	0.32	0.98	1.0000
250	250	0	40	0.32	0.98	1.0000
500	250	0	5	0.32	1.25	1.2150
500	250	0	40	0.32	1.87	1.9460
1000	250	0	5	0.32	2.05	2.0147
1000	250	0	40	0.32	3.82	3.9110
250	500	0	5	0.32	0.85	0.9194
250	500	0	40	0.32	0.58	0.5376
500	500	0	5	0.32	0.98	1.0000
500	500	0	40	0.32	1.00	1.0000
1000	500	0	5	0.32	1.37	1.3540
1000	500	0	40	0.32	1.92	1.9723
250	1000	0	5	0.32	0.76	0.8426
250	1000	0	40	0.32	0.36	0.2917
500	1000	0	5	0.32	0.81	0.8612
500	1000	0	40	0.32	0.54	0.5195

# Two Dimensional Model Output

Time Step = 0.003 seconds

Convergence Criteria = 0.001

<u>U0,cm/sec</u>	<u>U1,cm/sec</u>	<u>Theta</u>	<u>d, um</u>	<u>D, cm</u>	MODEL <u>Eff.</u>	UNIFIED <u>MODEL EFF</u>
1000	1000	0	5	0.32	0.98	1.0000
1000	1000	0	40	0.32	0.99	1.0000
250	125	30	5	0.32	0.87	1.0405
250	125	30	40	0.32	1.28	1.6996
0		30	0	0.32		ERR
500	125	30	40	0.32	2.63	3.4431
0		30	0	0.32		ERR
1000	125	30	40	0.32	5.58	6.9082
250	250	30	5	0.32	0.89	0.9918
250	250	30	40	0.32	0.72	0.8711
500	250	30	5	0.32	0.67	1.0796
500	250	30	40	0.32	1.32	1.7273
0		30	0	0.32		ERR
1000	250	30	40	0.32	2.79	3.4572
250	500	30	5	0.32	0.85	0.9595
250	500	30	40	0.32	0.43	0.4494
500	500	30	5	0.32	0.76	0.9842
500	500	30	40	0.32	0.74	0.8664
0		30	0	0.32		ERR
1000	500	30	40	0.32	1.55	1.7308
250	1000	30	5	0.32	0.81	0.9299
250	1000	30	40	0.32	0.30	0.2305
500	1000	30	5	0.32	0.77	0.9241
500	1000	30	40	0.32	0.45	0.4320
1000	1000	30	5	0.32	0.70	0.9704
1000	1000	30	40	0.32	0.81	0.8660
250	125	30	5	1	0.79	1.0130
250	125	30	40	1	0.75	1.5025
500	125	30	5	1	0.89	1.0825
500	125	30	40	1	0.90	3.1660
1000	125	30	0	1		1.3858
1000	125	30	40	1	4.09	6.7622
250	250	30	5	1	0.95	0.9973
250	250	30	40	1	0.63	0.9063
500	250	30	5	1	0.97	1.0260
500	250	30	40	1	1.05	1.6474
1000	250	30	0	1	0.53	1.1649
1000	250	30	40	1	2.16	3.3993
250	500	30	5	1	0.90	0.9863
250	500	30	40	1	0.48	0.5927
500	500	30	5	1	0.89	0.9947
500	500	30	40	1	0.66	0.8803
1000	500	30	0	1	0.85	1.0516
1000	500	30	40	1	1.17	1.7150
250	1000	30	5	1	0.87	0.9748
250	1000	30	40	1	0.41	0.4184

### Two Dimensional Model Output

Time Step = 0.003 seconds

Convergence Criteria = 0.001

<u>U0,cm/sec</u>	<u>Ui,cm/sec</u>	<u>Theta</u>	<u>d, um</u>	<u>D, cm</u>	<u>MODEL Eff.</u>	<u>UNIFIED MODEL EFF</u>
500	1000	30	5	1	0.87	0.9733
500	1000	30	40	1	0.45	0.4862
1000	1000	30	5	1	0.86	0.9896
1000	1000	30	40	1	0.69	0.8685

Uo = wind velocity

Ui = inlet velocity

theta = sampling angle

d = particle diameter

D = inlet diameter

3D RESULTS FOR SQUARE INLET OF 1/2 AREA = TO .5555 CM<sup>2</sup>  
 DIN = DIAMETER OF EQUAL AREA CIRCLE AND IS USED TO CALCULATE  
 STOKES NUMBER

INLET AREA: 0.56

UO	UI	THETA	DP	DT SEC	CVC	TRAJ AREA	BIEM Ai	UNIFIED Ai	% DIFF
1000	125	0	5	0.0003	0.001	0.112	1.6158	1.8193	-11%
1000	125	0	5	0.001	0.05	0.128	1.8483	1.8193	2%
1000	125	0	5	0.0003	0.05	0.191	2.7491	1.8193	51%
1000	125	0	40	0.0003	0.001	0.53	7.6309	7.2619	5%
1000	125	0	40	0.001	0.001	0.458	6.5928	7.2619	-9%
250	1000	0	5	0.001	0.01	1.733	0.7799	0.9500	-18%
250	1000	0	5	0.0005	0.05	1.928	0.8677	0.9500	-9%
250	1000	0	40	0.001	0.01	0.963	0.4334	0.3846	13%
250	1000	0	40	0.0005	0.01	0.944	0.4248	0.3846	10%
250	1000	0	40	0.0003	0.05	0.929	0.4183	0.3846	9%
1000	125	30	5	0.0003	0.01	0.053	0.7574	1.3243	-43%
1000	125	30	5	0.0005	0.05	0.056	0.8134	1.3243	-39%
1000	125	30	40	0.0005	0.05	0.488	7.0240	6.6768	5%
250	1000	30	5	0.002	0.05	1.654	0.7446	0.9786	-24%
250	1000	30	5	0.0005	0.05	1.933	0.8698	0.9786	-11%
250	1000	30	40	0.001	0.01	0.58	0.2611	0.4622	-44%
250	1000	30	40	0.0005	0.01	0.928	0.4177	0.4622	-10%
250	1000	30	40	0.0003	0.05	0.929	0.4183	0.4622	-10%
500	500	0	5	0.0005	0.05	0.57	1.0267	1.0000	3%
500	500	30	5	0.0005	0.05	0.554	0.9976	0.9955	0%
500	250	0	5	0.0005	0.05	0.314	1.1321	1.0686	6%
500	250	30	5	0.0005	0.05	0.305	1.0972	1.0219	7%
500	125	0	5	0.0005	0.05	0.209	1.5023	1.1936	26%
500	125	0	5	0.0005	0.05	0.172	1.2408	1.1936	4%
500	125	30	5	0.0005	0.05	0.164	1.1801	1.0693	10%
500	500	0	40	0.0005	0.05	0.573	1.0322	1.0000	3%
500	500	30	40	0.0005	0.05	0.528	0.9506	0.8856	7%
500	250	0	40	0.0005	0.05	0.544	1.9568	1.8251	7%
500	250	30	40	0.0005	0.05	0.496	1.7873	1.6177	10%
500	125	0	40	0.0005	0.05	0.516	3.7151	3.4445	8%
500	125	30	40	0.0005	0.05	0.439	3.1646	3.0644	3%

Uo = wind velocity

Ui = inlet velocity

theta = sampling angle

DP = particle diameter

DT = time step

cvc = convergence criteria

TRAJ AREA = area Ao in freestream

BIEM Ai = aspiration efficiency from model

UNIFIED Ai = aspiration efficiency from Hengal (1990)

## Two Dimensional Particle Tracking Program

C THIS PROGRAM COMBINES THE 2 DIMENSIONAL BIEM SOLUTION PROGRAM  
 C WRITTEN BY LIGGET AND LIU (1983) WITH THE ANALYTICAL SOLUTION  
 C TO THE PARTICLE EQUATIONS OF MOTION PROPOSED BY ALENIOUS  
 C (1989) TO PLOT PARTICLE TRAJECTORIES INTO AN INLET.  
 C

```

      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION RLN(100,100),RN(100,100),F(100),ID(100),
    $TITLE(20),CRITX(2),CRITY(2)
      COMMON H(100,100),RHS(100),N,X(100),Y(100),XXNOW,
    $YYNOW,P(100),PN(100),PN1(5),PN2(5),ICT(100),
    $DPDY(600),DPDX(600),A,L,N1,N2,UO,DIN,DP,THETA,UI,XCRIT
    $,YCRIT,DT,XXNEW,YYNEW,XNOW1,YNOW1
      READ (7,7) TITLE
    7 FORMAT (20A4)
      PRINT 7777,TITLE
    7777 FORMAT (//1X,20A4)
      READ (7,*) KEY
      READ (7,*) N
      MP=N
      N1=1
      IF (KEY .EQ. 1) PRINT 6933,N
    6933 FORMAT('  NUMBER OF NODES  =' ,I3/)
      IF (KEY .EQ. 1) PRINT 6938
    6938 FORMAT('.....KEY TO INPUT DATA AND ID NUMBERS.....
    1 '/' X,Y ARE THE NODAL COORDINATES '/' P,PN ARE THE
    2POTENTIAL AND THE NORMAL DERIVATIVE AT THE NODE')
      IF (KEY .EQ. 1) PRINT 6939
    6939 FORMAT ('  ID: IDENTIFIER FOR THE NODAL UNKNOWNNS' /,
    1 '                                =2 FOR P GIVEN' /,
    2 '                                =3 FOR PN GIVEN' /)
      IF (KEY .EQ. 1) PRINT 6941
    6941 FORMAT('  ICT: NODAL CORNER TYPE IDENTIFIER' /,
    1 '                                =1 FOR PN GIVEN APPROACHING NODE' /,
    2 '                                =2 FOR PN GIVEN LEAVING NODE' /,
    3 '.....ALL MOVEMENTS IN CLOCWISE SENSE.....' /)

```

C  
 C NODAL DATA I/O  
 C

```

    6932 L=N+1
      IF (KEY.EQ.1) PRINT 9953
    9953 FORMAT('  POINT',7X,'X-COOD',6X,'Y-COOD',5X,
    1'POTENTIAL',3X,'NORM DERV',3X,'ID',8X,'ICT')
      DO 6946 I=2,L
      READ (7,*) X(I),Y(I),P(I),PN(I),ID(I),ICT(I)
      IM1=I-1
    6946 IF (KEY.EQ.1) PRINT 9950,IM1,X(I),Y(I),P(I),PN(I),
    $ID(I),ICT(I)
    9950 FORMAT(I5,5X,F10.4,2X,F10.4,2X,F10.4,2X,F10.4,2X,I5,
    15X,I5)

```

C

C CLEARING THE GLOBAL MATRIX

C

```
DO 17 I=1,N
DO 16 J=1,L
16 H(I,J)=0.0
17 F(I)=0.0
```

C

C

C

BOUNDARY INTEGRATION

```
X(1)=X(L)
X(L+1)=X(2)
Y(1)=Y(L)
Y(L+1)=Y(2)
DO 200 I=2,L
II1=1
II2=1
PNJP=0.0
PJP=0.0
DO 140 J=2,L
IF(I.EQ.J) GOTO 130
IF(I.EQ.J+1) GOTO 135
IF(J.NE.L) GOTO 98
IF(I.EQ.2) GO TO 135
98 R1=DSQRT((X(J+1)-X(J))**2+(Y(J+1)-Y(J))**2)
CO=(X(J+1)-X(J))/R1
SI=(Y(J+1)-Y(J))/R1
XIA=(Y(J)-Y(I))*SI+(X(J)-X(I))*CO
XIB=(Y(J+1)-Y(I))*SI+(X(J+1)-X(I))*CO
ETA=DABS((Y(I)-Y(J))*CO-(X(I)-X(J))*SI)
100 IF(ETA.LT.1.E-5) GO TO 102
BTN=DATAN(XIB/ETA)
ATN=DATAN(XIA/ETA)
105 ASQ=XIA**2+ETA**2
ALN=DLOG(ASQ)
BSQ=XIB**2+ETA**2
106 BLN=DLOG(BSQ)
107 ONE=BSQ*(BLN-1.)-ASQ*(ALN-1.)
TWO=XIB*BLN-XIA*ALN-2.*(XIB-XIA)+2.*ETA*(BTN-ATN)
SIGNRN=-(X(J)-X(I))*(Y(J+1)-Y(J))+(X(J+1)-X(J))*(Y(J)-
$Y(I))
PJ=(XIB*(BTN-ATN)-.5*ETA*(BLN-ALN))/(XIB-XIA)
PJ=DSIGN(PJ,SIGNRN)
XBXA=DABS(XIB-XIA)
PNJ=TWO*XIB/(2.*XBXA)-ONE/(4.*XBXA)
IF(ICT(J).NE.1) GOTO 321
PN1(II1)=PN(J)
F(I-1)=F(I-1)+PNJP*PN(J)
II1=II1+1
PNJP=0.0
321 IF(ICT(J).NE.2) GOTO 432
F(I-1)=F(I-1)+PNJ*PN(J)
PN2(II2)=PN(J)
II2=II2+1
PNJ=0.0
```

```

432 RN(I,J)=PJ+PJP
    RLN(I,J)=PNJ+PNJP
    PJP=(ETA*(BLN-ALN)*0.5-XIA*(BTN-ATN))/(XIB-XIA)
    PJP=DSIGN(PJP,SIGNRN)
    PNJP=ONE/(4.*XBXA)-TWO*XIA/(2.*XBXA)
    GO TO 140
102 BTN=0.0
    ATN=0.0
    GO TO 105
130 ALN=0.0
    BTN=0.0
    ATN=0.0
    XIB=DSQRT((X(I+1)-X(I))**2+(Y(I+1)-Y(I))**2)
    XIA=0.0
    ETA=0.0
    ASQ=0.0
    BSQ=XIB**2
    GO TO 106
135 XIA=-DSQRT((X(I)-X(J))**2+(Y(I)-Y(J))**2)
    BTN=0.0
    ATN=0.0
    XIB=0.0
    BLN=0.0
    BSQ=0.0
    ASQ=XIA**2
    ALN=DLOG(ASQ)
    ETA=0.0
    GOTO 107
140 CONTINUE
    RN(I,2)=RN(I,2)+PJP
    IF(ICT(2).NE.1) GOTO 544
    F(I-1)=F(I-1)+PNJP*PN1(1)
    PNJP=0.0
544 RLN(I,2)=RLN(I,2)+PNJP
    ALPHA=((X(I)-X(I-1))**2+(Y(I)-Y(I-1))**2+
    $(X(I)-X(I+1))**2+(Y(I)-Y(I+1))**2-(X(I+1)-
    $ X(I-1))**2-(Y(I+1)-Y(I-1))**2)/(2.*DSQRT(((X(I)
    $-X(I-1))**2+(Y(I)-Y(I-1))**2)*((X(I)-X(I+1)
    $)**2+(Y(I)-Y(I+1))**2))))
    IF(DABS(ALPHA).LT.0.9999) GOTO 141
    ALPHA=3.14159265
    GOTO 170
141 ALPHA=DACOS(ALPHA)
    IF (DABS(X(I)-X(I-1)).GT.1.E-5) GOTO 144
    IF(Y(I).LT.Y(I-1)) GOTO 142
    IF(X(I+1).LT.X(I)) ALPHA=6.28318531-ALPHA
    GOTO 170
142 IF (X(I+1).GT.X(I)) ALPHA=6.28318531-ALPHA
    GOTO 170
144 A=(Y(I-1)-Y(I))/(X(I-1)-X(I))
    B=Y(I)-A*X(I)
    YA=A*X(I+1)+B
    IF(Y(I) .LT. Y(I-1)) GOTO 150
    IF(X(I) .LT. X(I-1)) GOTO 146

```

```

        IF(YA .LT. Y(I+1))ALPHA=6.28318531-ALPHA
        GOTO 170
146  IF(YA .GT. Y(I+1))ALPHA=6.28318531-ALPHA
        GOTO 170
150  IF(X(I) .GT. X(I-1)) GOTO 152
        IF(YA .GT. Y(I+1))ALPHA=6.28318532-ALPHA
        GOTO 170
152  IF(YA .LT. Y(I+1))ALPHA=6.28318531-ALPHA
170  RN(I,I)=-ALPHA
200  CONTINUE
    13  FORMAT(//)
C
C      ASSEMBLING THE GLOBAL EQUATIONS
C
    DO 1000 I=1,N
    DO 2000 J=1,N
    IF(ID(J+1) .EQ. 2)H(I,J)=-RLN(I+1,J+1)
    IF(ID(J+1) .EQ. 3)H(I,J)=RN(I+1,J+1)
2000 CONTINUE
C
C      COMPUTING R-H-S VECTOR
C
    A=0.0
    DO 2001 J=1,N
    IF(ICT(J) .NE. 0)PN(J+1)=0.0
2001  A=A-P(J+1)*RN(I+1,J+1)+PN(J+1)*RLN(I+1,J+1)
        H(I,L)=A+F(I)
1000 CONTINUE
C
C      SOLVING GLOBAL EQS FOR NODAL UNKNOWNNS
C
    CALL EQSOL
C
C      ALLOCATING EACH SOLUTION TO THE PROPER NODAL UNKNOWN
C
    JJ1=1
    DO 8003 J=2,L
    IF(ID(J) .EQ. 2) GOTO 8005
    P(J)=RHS(JJ1)
    JJ1=JJ1+1
    GOTO 8003
8005  PN(J)=RHS(JJ1)
        JJ1=JJ1+1
8003 CONTINUE
C
C      OUTPUT BOUNDARY SOLUTION
C
    WRITE (6,13)
    WRITE (6,30)
30  FORMAT('.....COMPUTED RESULTS.....')
        do 7654 j=2,l
        write (6,*) j-1,pn(j),p(j)
7654 continue
C

```

```

C      PERFORM TRAJECTORY CALCULATION
C
C      INPUT PARTICLE AND AIRSTREAM VARIABLES AND CONV. PARAMETERS
C
      DO 4000 K=1,2
        IF (K .EQ. 1) THEN
          A=1.
        ELSE IF (K .EQ. 2) THEN
          A=-1.
        ELSE
          ENDIF
        CALL PART
        CRITX(K)=XCRIT
        CRITY(K)=YCRIT
4000 CONTINUE
      EFF = (((CRITX(1)-CRITX(2))**2+(CRITY(1)-CRITY(2))**2)**.5
      $*(-1)*UO)/(UI*DIN)
      WRITE (3,*) UO,UI,DP,DIN,THETA,EFF
      PRINT *, EFF
      STOP
      END

C
C      LINEAR EQUATION SOLVER SUBROUTINE
C
      SUBROUTINE EQSOL
      IMPLICIT REAL *8(A-H,O-Z)
      DIMENSION M(100)
      COMMON A(100,100),X(100),N,X1(100),Y(100),XXNOW,
      $YYNOW,P(100),PN(100),PN1(5),PN2(5),ICT(100),
      $DPDY(600),DPDX(600),A1,L,N1,N2,UO,DIN,DP,THETA,UI
      $,XCRIT,YCRIT,DT,XXNEW,YYNEW,XNOW1,YNOW1
      DO 5 I=1,N
        M(I)=1
        AMAX=A(I,1)
        DO 2 J=2,N
          IF(DABS(A(I,J)) .LE. DABS(AMAX)) GOTO 2
100    AMAX=A(I,J)
        M(I)=J
      2 CONTINUE
        IF(AMAX .EQ. 0) GOTO 98
      3 NN=N+1
        DO 4 J=1,NN
          A(I,J)=A(I,J)/AMAX
          DO 5 IP=1,N
            IF(IP .EQ. I) GOTO 5
            MMM=M(I)
            ZMULT=A(IP,MMM)
            DO 6 J=1,NN
              IF(J .NE. MMM) GOTO 9
            8 A(IP,J)=0.0
              GOTO 6
            9 A(IP,J)=A(IP,J)-ZMULT*A(I,J)
          6 CONTINUE
        5 CONTINUE

```

```

      DO 7 I=1,N
      NO=M(I)
      7 X(NO)=A(I,NN)
      RETURN
98  CONTINUE
      STOP
      END

```

C  
C  
C

SUBROUTINE FOR PARTICLE TRAJ. CALC., 2D

SUBROUTINE PART

```

      IMPLICIT REAL *8(A-H,O-Z)
      DIMENSION DPDXOL(600),DPDYOL(600),MAXI(150)
      COMMON H(100,100),RHS(100),N,X(100),Y(100),XXNOW,
$YYNOW,P(100),PN(100),PN1(5),PN2(5),ICT(100),
$DPDY(600),DPDX(600),A,L,N1,N2,UO,DIN,DP,THETA,UI
$,XCRIT,YCRIT,DT,XXNEW,YYNEW,XNOW1,YNOW1

```

C C C C C C C C C C C C C C C C

VARIABLE IDENTIFICATION

UO = INITIAL FREE STREAM VELOCITY

G = GRAVITY

DP = PARTICLE DIAMETER, CM

AV = AIR VISCOSITY

DIN = INLET DIAMETER

DT = TIME STEP LENGTH

PDENS = PARTICLE DENSITY

ADENS = AIR DENSITY

VR = PARTICLE RELATIVE VELOCITY

RE = REYNOLDS NUMBER

DPDX, DPDY = AIR VELOCITY COMPONENTS

VXP, VYP = PARTICLE VELOCITY COMPONENTS

XX, YY = PARTICLE LOCATION COORDINATES

THETA = NOZZLE ANGLE

```
READ (8,*) UO,DP,DIN,DT,THETA,UI,XDIN
```

```
READ (8,*) CVC
```

```
PRINT *, UO, DP, DIN, DT, THETA, UI, XDIN, CVC
```

$$G = -980.$$
$$dt_1 = dt$$
 $AV = .000183$ 

PDENS=1.0

ADENS=.001205

$$DPL = 10000.0 * DP$$
$$CC=1+((2.*0.07/DPL)*(1.257+(0.4*EXP(-0.55*DPL/0.07))))$$
$$TAU = (DP^{**}2 * PDENS * CC) / (18 * AV)$$
$$\text{THETA1} = -.01745277 * \text{THETA}$$
$$\text{THETA} = .01745277 * \text{THETA}$$
$$GX = G * \sin(\theta)$$
$$GY = G * \cos(\text{THETA})$$

MANY=599

N MANY=50

$$N_2 = 0$$

```
IF (A .GT. 0.) THEN
```

```

YYNOW=XDIN*DIN*SIN(THETA1)
XXNOW=XDIN*DIN*COS(THETA)
ELSE
YYNOW= XDIN*DIN*SIN(THETA1)+(.67*XDIN*DIN*COS(THETA)*A)
XXNOW=XDIN*DIN*COS(THETA)+(.67*XDIN*DIN*SIN(THETA)*A)
ENDIF
NCAPF=0
IF (A .GT. 0) NFCAP=0
NMISS=0
CONV=9999
N1=1

```

C  
C  
C

# PARTICLE POSITION AND VELOCITY COMPONENTS

```

DO 5000 J=1,NMANY
  NCAP=0
  N1=1
  N2=N2+1
  DO 4300 I=1,MANY
    CALL INSOLN
    IF (I .EQ. 1) THEN
      VXNOW=DPDX(I)+(TAU*GX)
      VYNOW=DPDY(I)+(TAU*GY)
    ENDIF
    VR=((VXNOW-DPDX(I))**2+(VYNOW-DPDY(I))**2)**0.5
    RE=VR*DP*ADENS/AV
    IF (RE .LE. 0.5) THEN
      QRE=1
    ELSE IF ((RE .GT. 0.5) .AND. (RE .LE. 800.)) THEN
      QRE=1+(0.15*RE**0.687)
    ELSE
      QRE=0.44*RE/24
    ENDIF
    IF (I .EQ. 1) THEN
      DPDXOL(I)=DPDX(I)
      DPDYOL(I)=DPDY(I)
    ELSE
      DPDXOL(I)=DPDX(I-1)
      DPDYOL(I)=DPDY(I-1)
    ENDIF
    if ((xxnow .lt. 1.5*din) .and. (xxnow .gt. -1.5*din)
$      .and. (yynew .lt. 1.5*din) .and.
$      (yynew .gt. -1.5*din)) then
      dt=dt1/10.
    else
      dt=dt1
    endif
    UAX=(DPDX(I)-DPDXOL(I))/DT
    UAY=(DPDY(I)-DPDYOL(I))/DT
    UBX=DPDX(I)-((UAX-GX)*(TAU/QRE))
    UBY=DPDY(I)-((UAY-GY)*(TAU/QRE))
    VXNEW=(UAX*DT)+UBX-((UBX-VXNOW)*
$      EXP(-QRE*DT/TAU))

```

```

VYNEW=(UAY*DT)+UBY-((UBY-VYNOW)*
$   EXP(-QRE*DT/TAU))
XXNEW=XXNOW+(UAX/2*DT**2)+(UBX*DT)-
$   ((UBX-VXNOW)*(TAU/QRE)*(1-EXP(-QRE*DT/TAU)))
YYNEW=YYNOW+(UAY/2*DT**2)+(UBY*DT)-
$   ((UBY-VYNOW)*(TAU/QRE)*(1-EXP(-QRE*DT/TAU)))
IF (I .EQ. 1) THEN
XNOW1=XXNOW
YNOW1=YYNOW
ENDIF
5002 WRITE (4,5002) XXNOW,YYNOW
      FORMAT (2F15.10)
      IF (XXNEW .LT. -1.1*XDIN/2*DIN) THEN
        NCAP=2
        PRINT *, 'PARTICLE EXIT REAR BOUNDARY, MISS'
        GOTO 4301
      ELSE IF ((YYNEW .GT. 1.1*XDIN*DIN) .OR. (YYNEW .LT.
$      -1.1*XDIN*DIN)) THEN
        NCAP=2
        PRINT *, 'PARTICLE EXIT TOP/BOTTOM, MISS'
        GOTO 4301
      ELSE IF ((XXNEW .LT. 0.0) .AND. (XXNOW .GT. 0.0)
$      .AND. (ABS(YYNEW) .LT. DIN/2)) THEN
        NCAP=1
        PRINT *, 'CAPTURE AT FACE'
        GOTO 4301
      ELSE IF ((ABS(YYNEW) .LT. DIN/2) .AND.
$      (ABS(YYNOW) .GT. DIN/2) .AND. (XXNEW .LT. 0))
$      THEN
        NCAP=2
        PRINT *, 'CONTACT TUBE, MISS'
        GOTO 4301
      ELSE
        NCAP=0
      ENDIF
      N1=N1+1
      XXNOW=XXNEW
      YYNOW=YYNEW
      VXNOW=VXNEW
      VYNOW=VYNEW
4300 CONTINUE
      PRINT *, 'ERROR, DID NOT EXIT LOOP'
      PRINT *, XNOW1,YNOW1,N1
4301 CONTINUE
      MAXI(J)=N1
      IF (NFCAP .GT. 0) THEN
        GOTO 50
      ELSE IF (NCAP .EQ. 1) THEN
        NFCAP=1
        YCAP=YNOW1
        XCAP=XNOW1
        YYNOW=YNOW1+(.67*XDIN*DIN*COS(THETA))
        XXNOW=XNOW1-((YNOW1-YYNOW)*TAN(THETA))
        GOTO 4999

```

```

ELSE IF ((NCAP .EQ. 2) .AND. (YYNOW .LE. -DIN/2.)) THEN
  YYNOW=YNOW1+(.1*DIN)
  XXNOW=XNOW1+((YYNOW-YNOW1)*TAN(THETA))
  GOTO 4999
ELSE IF ((NCAP .EQ. 2) .AND. (YYNOW .GE. DIN/2.)) THEN
  YYNOW=YNOW1-(.1*DIN)
  XXNOW=XNOW1-((YNOW1-YYNOW)*TAN(THETA))
  GOTO 4999
ELSE
ENDIF
50 IF (NMISS .GT. 0) THEN
  GOTO 10
ELSE IF (NCAP .EQ. 2) THEN
  NMISS=1
  YMISS=YNOW1
  XMISS=XNOW1
  GOTO 10
ELSE IF (NCAP .EQ. 1) THEN
  YYNOW=YNOW1+(A*.1*DIN)
  XXNOW=XNOW1+((YYNOW-YNOW1)*TAN(THETA))
  XDIN=XDIN+(.1*XDIN)
  GOTO 4999
ELSE
ENDIF
10 IF (NCAP .EQ. 1) THEN
  YCAP=YNOW1
  XCAP=XNOW1
ELSE IF (NCAP .EQ. 2) THEN
  YMISS=YNOW1
  XMISS=XNOW1
ELSE
ENDIF
CONV=((XMISS-XCAP)**2+(YMISS-YCAP)**2)**.5
IF (YCAP .GT. YMISS) THEN
  YYNOW=(CONV/2*COS(THETA))+YMISS
  XXNOW=(CONV/2*SIN(THETA))+XMISS
ELSE IF (YMISS .GT. YCAP) THEN
  YYNOW=(CONV/2*COS(THETA))+YCAP
  XXNOW=(CONV/2*SIN(THETA))+XCAP
ELSE
ENDIF
IF (CONV .LT. CVC) THEN
  XCRIT=XXNOW
  YCRIT=YYNOW
  GOTO 5001
ELSE
ENDIF
4999 PRINT *, N2,NCAP,YNOW1,DPDX(1),DPDY(1)
5000 CONTINUE
5001 PRINT *, 'TRAJECTORIES HAVE CONVERGED'
PRINT *, UC,DP,DIN,THETA,XCRIT,YCRIT
RETURN
STOP
END

```

```

C
C      SUBROUTINE TO CALC. VELOCITY AT PARTICLE LOCATION
C
      SUBROUTINE INSOLN
      IMPLICIT REAL *8(A-H,O-Z)
      DIMENSION U(600)
      COMMON H(100,100),RHS(100),N,X(100),Y(100),XXNOW,
$YYNOW,P(100),PN(100),PN1(5),PN2(5),ICT(100),
$DPDY(600),DPDX(600),A,L,N1,N2,UO,DIN,DP,THETA,UI,
$XCRIT,YCRIT,DT,XXNEW,YYNEW,XNOW1,YNOW1
C
C      PERFORMING BOUNDARY INTEG. FOR INTERNAL SOLUTION
C
      DO 4200 I=N1,N1
      II1=1
      II2=1
      U(I)=0.0
      DPDX(I)=0.0
      DPDY(I)=0.0
      PNJP=0.0
      PNXP=0.0
      PNYJP=0.0
      PJP=0.0
      PXJP=0.0
      PYJP=0.0
      DO 4140 J=2,L
      R2=DSQRT((X(J+1)-X(J))**2+(Y(J+1)-Y(J))**2)
      CO=(X(J+1)-X(J))/R2
      SI=(Y(J+1)-Y(J))/R2
      ETA=DABS((YYNOW-Y(J))*CO-(XXNOW-X(J))*SI)
      XIA=(Y(J)-YYNOW)*SI+(X(J)-XXNOW)*CO
      XIB=(Y(J+1)-YYNOW)*SI+(X(J+1)-XXNOW)*CO
      XBXA=XIB-XIA
      SIGNRN=-(X(J)-XXNOW)*(Y(J+1)-Y(J))+(X(J+1)-X(J))*(Y(J)
$ -YYNOW)
      IF(SIGNRN .LT. 0)ETA=-ETA
      IF(DABS(ETA) .LT. 1.E-5) GOTO 4102
      BTN=DATAN(XIB/ETA)
      ATN=DATAN(XIA/ETA)
      GOTO 4105
4102  BTN=0.0
      ATN=0.0
4105  ASQ=XIA**2+ETA**2
      ALN=DLOG(ASQ)
      BSQ=XIB**2+ETA**2
      BLN=DLOG(BSQ)
      ONE=BSQ*(BLN-1.)-ASQ*(ALN-1.)
      TWO=XIB*BLN-XIA*ALN-2.*(XIB-XIA)+2.*ETA*(BTN-ATN)
      PJ=(XIB*(BTN-ATN)-0.5*ETA*(BLN-ALN))/(XIB-XIA)
      PXJ=(-0.5*SI*(BLN-ALN+2.)-CO*(BTN-
$ ATN)+SI*(ETA**2+XIA*XIB)/ASQ)/(XIB-XIA)+ETA*CO/ASQ
      PYJ=(0.5*CO*(BLN-ALN+2.)-SI*(BTN- ATN)-CO*(ETA**2+XIA*
$ XIB)/ASQ)/(XIB-XIA)+ETA*SI/ASQ
      PNJ=TWO*XIB/(2.*XBXA)-ONE/(4.*XBXA)

```

```

PNXJ=-CO+((ETA*CO-XIB*SI)*(BTN-ATN)+0.5*(XIB*CO+ETA
$*SI)*(BLN-ALN))/XBXA
PNYJ=-SI+((ETA*SI+XIB*CO)*(BTN-ATN)+0.5*(XIB*SI-
$ETA*CO)*(BLN-ALN))/XBXA
IF(ICT(J) .NE. 1) GOTO 4321
U(I)=U(I)-PNJP*PN1(II1)
DPDX(I)=DPDX(I)+PNXJP*PN1(II1)
DPDY(I)=DPDY(I)+PNYJP*PN1(II1)
II1=II1+1
PNJP=0.0
PNXJP=0.0
PNYJP=0.0
4321 IF(ICT(J) .NE. 2) GOTO 4322
U(I)=U(I)-PNJ*PN2(II2)
DPDX(I)=DPDX(I)+PNXJ*PN2(II2)
DPDY(I)=DPDY(I)+PNYJ*PN2(II2)
II2=II2+1
PNJ=0.0
PNXJ=0.0
PNYJ=0.0
4322 U(I)=U(I)+(PJ+FJP)*P(J)-(PNJ+PNJP)*PN(J)
DPDX(I)=DPDX(I)+(PXJ+PXJP)*P(J)+(PNXJ+PNXJP)*PN(J)
DPDY(I)=DPDY(I)+(PYJ+PYJP)*P(J)+(PNYJ+PNYJP)*PN(J)
PJP=(ETA*(BLN-ALN)*0.5-XIA*(BTN-ATN))/(XIB-XIA)
PXJP=(0.5*SI*(BLN-ALN-2.)+CO*(BTN-ATN)+SI*(ETA**2+
$XIA*XIB)/BSQ)/(XIB-XIA)-ETA*CO/BSQ
PYJP=(-0.5*CO*(BLN-ALN-2.)+SI*(BTN-ATN)-CO*(ETA**2+
$XIA*XIB)/BSQ)/(XIB-XIA)-ETA*SI/BSQ
PNJP=ONE/(4.*XBXA)-TWO*XIA/(2.*XBXA)
PNXJP=CO+((-ETA*CO+XIA*SI)*(BTN-ATN)-0.5*(XIA*CO+ETA*
$SI)*(BLN-ALN))/XBXA
PNYJP=SI+(-(ETA*SI+XIA*CO)*(BTN-ATN)-0.5*(XIA*SI-ETA*
$CO)*(BLN-ALN))/XBXA
4140 CONTINUE
U(I)=U(I)+PJP*P(2)
DPDX(I)=DPDX(I)+PXJP*P(2)
DPDY(I)=DPDY(I)+PYJP*P(2)
IF(ICT(2) .NE. 1) GOTO 4195
U(I)=U(I)-PNJP*PN1(1)
DPDX(I)=DPDX(I)+PNXJP*PN1(1)
DPDY(I)=DPDY(I)+PNYJP*PN1(1)
PNJP=0.0
PNXJP=0.0
PNYJP=0.0
4195 CONTINUE
U(I)=U(I)-(PNJP*PN(2))
DPDX(I)=DPDX(I)+PNXJP*PN(2)
DPDY(I)=DPDY(I)+PNYJP*PN(2)
U(I)=U(I)/6.283185308
DPDX(I)=DPDX(I)/6.283185308
DPDY(I)=DPDY(I)/6.283185308
4200 CONTINUE
RETURN
END

```

### Three Dimensional Model Programs:

PROGRAM 4PTGQ.F

```

C
C   THIS IS A PROGRAM TO CALCULATE THE THREE DIMENSIONAL
C   VELOCITY FIELD INTO LOCAL EXHAUST OPENINGS USING THE
C   BIEM METHOD. WRITTEN BY MIKE FLYNN IN CONJUNCION
C   WITH CASEY MILLER IN MARCH 1988
C
C
C   IMPLICIT REAL*8(A-H,O-Z)
C   DIMENSION PHI(367),DPHI(367),ALPHA(367),
C   1ID(367),PREV(3),AE(691),VX(100),VY(100),VZ(100),R(367),
C   2H(367,367),U(367),X(367),Y(367),Z(367),NE(691,4),ICT(367),
C   3XX(100),YY(100),ZZ(100),ALTDPHI(691,3)
C   COMMON H,U,MP,X,Y,Z,NE,XX,YY,ZZ,I,J,K,L,A,B,AE
C   OPEN (5,FILE='INPUT.DAT')
C   OPEN (3,FILE='INDAT2')
C   OPEN (6,FILE='PRN')
C   READ (5,*) N
C   READ (5,*) M
C   LL=N+1
C   MP=N
C   DO 1001 I=1,N
C   READ (5,*) X(I), Y(I), Z(I), PHI(I), DPHI(I), ID(I), ICT(I)
1001 CONTINUE
C   READ (5,*)((NE(I,II),II=1,4),I=1,M)
C   PRINT *, NE(691,1), NE(691,2), NE(691,3), NE(691,4)
C   CLOSE (3)
C
C
C   THE I LOOP GENERATES VALUES FOR THE COEFFICIENT MATRIX
C   H AND THE KNOWN COLUMN VECTOR R. DIFFERENT VALUES FOR I
C   CORRESPOND TO THE BASE POINT BEING POSITIONED AT A
C   DIFFERENT NODE. VALUES FOR THE UNKNOWN COLUMN VECTOR
C   U ARE ALLOCATED DEPENDING ON THE ID CODE AT THE START
C   OF THE LOOP
C
C
C   DO 10 I=1,N
C   R(I)=0.0
C   DO 20 J=1,N
C   H(I,J)=0.0
20 CONTINUE
10 CONTINUE
C   DO 100 I=1,N
C   IF(ID(I).EQ.1) THEN
C   U(I)=DPHI(I)
C   ELSE
C   U(I)=PHI(I)
C   ENDIF
C   ALPHA(I)=0.0

```

```

C
C   THE J LOOP CONTAINS THE SUMMATIONS OVER EACH ELEMENT
C   INITIALLY THE AREA OF THE JTH ELEMENT IS CALCULATED
C   THIS IS AE(J).
C
DO 200 J=1,M
  DY21=Y(NE(J,2))-Y(NE(J,1))
  DY31=Y(NE(J,3))-Y(NE(J,1))
  DZ21=Z(NE(J,2))-Z(NE(J,1))
  DZ31=Z(NE(J,3))-Z(NE(J,1))
  DX21=X(NE(J,2))-X(NE(J,1))
  DX31=X(NE(J,3))-X(NE(J,1))
  AE1=DY21*DZ31-DZ21*DY31
  AE2=DZ21*DX31-DX21*DZ31
  AE3=DX21*DY31-DY21*DX31
  AE(J)=0.5*(DSQRT(AE1**2+AE2**2+AE3**2))
  ASUM=0.0
C
C
C   THE K LOOP CALLS THE PROGRAMS THAT PERFORM THE BOUNDARY
C   INTEGRATIONS FOR A SINGLE TRIANGULAR ELEMENT, SPINT
C   IS USED IF THE BASE POINT COINCIDES WITH THE ELEMENT
C   NODE THAT IS BEING CONSIDERED, GQUAD IS THE STANDARD
C   GAUSSIAN QUADRATURE. BOTH PROGRAMS RETURN A AND B.
C
C
DO 300 K=1,3
  IF(I.EQ.NE(J,K)) THEN
    CALL SPINT
  ELSE
    CALL GQUAD
  ENDIF
  IF(ID(NE(J,K)).EQ.1.AND.ICT(NE(J,K)).EQ.0) THEN
    H(I,NE(J,K))=H(I,NE(J,K))-B
    R(I)=R(I)-A*PHI(NE(J,K))
  ELSEIF(ICT(NE(J,K)).EQ.1.AND.ID(NE(J,K)).EQ.1.AND.
$ ID(NE(J,4)).EQ.2) THEN
    H(I,NE(J,K))=H(I,NE(J,K))
    R(I)=R(I)+B*DPHI(NE(J,4))-A*PHI(NE(J,K))
    ALTDPHI(J,K)=DPHI(NE(J,4))
  ELSEIF(ICT(NE(J,K)).EQ.1.AND.ID(NE(J,K)).EQ.1.AND.
$ ID(NE(J,4)).EQ.1) THEN
    H(I,NE(J,K))=H(I,NE(J,K))-B
    R(I)=R(I)-A*PHI(NE(J,K))
  ELSE
    H(I,NE(J,K))=H(I,NE(J,K))+A
    R(I)=R(I)+B*DPHI(NE(J,K))
  ENDIF
  ASUM=ASUM+A
C
C
300 CONTINUE
  ALPHA(I)=-ASUM+ALPHA(I)
200 CONTINUE

```

```

      IF(ID(I).EQ.1) THEN
        R(I)=R(I)-ALPHA(I)*PHI(I)
      ELSE
        H(I,I)=H(I,I)+ALPHA(I)
      ENDIF
100  CONTINUE
      DO 111 I=1,N
        H(I,LL)=R(I)
111  CONTINUE
      CALL EQSOL

C
C   AFTER RETURNING FROM EQSOL U(I) HAS BEEN WRITTEN
C   OVER WITH THE SOLUTIONS, THESE ARE THEN ALLOCATED TO
C   PHI(I) OR DPHI(I) AS FOLLOWS:
C
C   OPEN (4,FILE='BOUND.OUT')
      DO 1000 I=1,N
        IF(ID(I).EQ.1) THEN
          DPHI(I)=U(I)
        ELSE
          PHI(I)=U(I)
        ENDIF
        WRITE (6,678) X(I),Y(I),Z(I),PHI(I),DPHI(I),ID(I),ICT(I)
678   FORMAT (F15.5,' ',F15.5,' ',F15.5,' ',F15.5,' ',F15.5,' ',
      $I5,' ',I5)
1000  CONTINUE
      CLOSE (4)

C
C   READ IN THE INTERNAL POINTS FOR VELOCITY CALCULATIONS
C
      READ (5,*) NN
      DO 222 I=1,NN
        READ (5,*) XX(I), YY(I), ZZ(I)
222  CONTINUE

C
C   DECLARE AND INITIALIZE
C
      DO 1100 I=1,NN
        PVX=0.0
        PVY=0.0
        PVZ=0.0
      DO 2000 J=1,M
        PREVX=0.0
        PREVY=0.0
        PREVZ=0.0
      DO 3000 K=1,3
      DO 4000 L=1,3
        CALL INTERGQ
        IF (ICT(NE(J,K)).EQ.1.AND.ID(NE(J,K)).EQ.1
      $ .AND.ID(NE(J,4)).EQ.2) THEN
          DPHIDE=ALTDPHI(J,K)
        ELSE
          DPHIDE=DPHI(NE(J,K))
        ENDIF

```

```

PREV(L)=(A*PHI(NE(J,K))-B*DPHIDE)
4000 CONTINUE
PREVX=PREVX+PREV(1)
PREVY=PREVY+PREV(2)
PREVZ=PREVZ+PREV(3)
3000 CONTINUE
PVX=PVX+PREVX
PVY=PVY+PREVY
PVZ=PVZ+PREVZ
2000 CONTINUE
COEF1=-0.079577471
VX(I)=COEF1*PVX
VY(I)=COEF1*PVY
VZ(I)=COEF1*PVZ
1100 CONTINUE
C
C
C   OUTPUT INTERNAL DATA TO FILE
C   print *, 'internal velocities:'
C
C   OPEN (4,FILE='INT.OUT')
C   DO 444 I=1,NN
C     WRITE (6,*) VX(I),VY(I),VZ(I)
444 CONTINUE
C   CLOSE (4)
C   CONTINUE
C   STOP
C   END
C
C
SUBROUTINE GQUAD
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION W(13),CHI(13),ETA(13),F(13),
1H(367,367),U(367),X(367),Y(367),Z(367),
2NE(691,4),XX(100),YY(100),ZZ(100),AE(691)
COMMON H,U,MP,X,Y,Z,NE,XX,YY,ZZ,I,J,K,L,A,B,AE
A=0.D00
B=0.D00
W(1)=-0.5626000000000000
W(2)=.5208333333333333
W(3)=W(2)
W(4)=W(2)
CHI(1)=.3333333333333333
CHI(2)=.6000000000000000
CHI(3)=.2000000000000000
CHI(4)=CHI(3)
ETA(1)=CHI(1)
ETA(2)=CHI(3)
ETA(3)=CHI(2)
ETA(4)=CHI(3)
DO 4400 II=1,4
IF(K.EQ.1) THEN
F(II)=CHI(II)
ELSEIF (K.EQ.2) THEN

```

```

      F(II)=ETA(II)
    ELSE
      F(II)=1.D00-ETA(II)-CHI(II)
    ENDIF
    A1=(X(NE(J,1))*CHI(II)+X(NE(J,2))*ETA(II)+X(NE(J,3))
    $*(1.D00-CHI(II)-ETA(II))-X(I))
    B1=(Y(NE(J,1))*CHI(II)+Y(NE(J,2))*ETA(II)+Y(NE(J,3))
    $*(1.D00-CHI(II)-ETA(II))-Y(I))
    C1=(Z(NE(J,1))*CHI(II)+Z(NE(J,2))*ETA(II)+Z(NE(J,3))
    $*(1.D00-CHI(II)-ETA(II))-Z(I))
    R=DSQRT(A1**2+B1**2+C1**2)
    FF=F(II)*(1.D00/R)*W(II)
    B=B+FF
    IF (I.EQ.NE(J,1).OR.I.EQ.NE(J,2).OR.I.EQ.NE(J,3)) THEN
      GOTO 4400
    ELSE
      CONTINUE
    ENDIF
    AY1=Y(NE(J,1))-B1-Y(I)
    AY2=Y(NE(J,2))-B1-Y(I)
    AZ1=Z(NE(J,1))-C1-Z(I)
    AZ2=Z(NE(J,2))-C1-Z(I)
    AX1=X(NE(J,1))-A1-X(I)
    AX2=X(NE(J,2))-A1-X(I)
    A2=AY1*AZ2-AZ1*AY2
    B2=AZ1*AX2-AX1*AZ2
    C2=AX1*AY2-AY1*AX2
    G1=A1*A2+B1*B2+C1*C2
    G2=DSQRT(A2**2+B2**2+C2**2)
    G=F(II)*W(II)*(-G1/(R**3*G2))
    A=A+G
4400 CONTINUE
    A=AE(J)*A
    B=AE(J)*B
    RETURN
  END

```

C  
C  
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C  
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C  
C  
C  
C  
C

NOTE THE SIGN FOR G IS CORRECT HERE ONLY IF  
THE ELEMENTS HAVE BEEN NUMBERED COUNTERCLOCKWISE  
WHEN LOOKING OUT OF THE DOMAIN THIS CONVENTION  
MUST BE OBSERVED WHEN CREATING E(J,K)

THE SUBROUTINE SPINT IS DESIGNED TO HANDLE THE SPECIAL  
INTEGRATIONS THAT OCCUR WHEN AN ELEMENT NODE COINCIDES  
WITH THE BASE POINT

```

SUBROUTINE SPINT
  IMPLICIT REAL*8(A-H,O-Z)
  DIMENSION W(13),ETA(13),CHI(13),F(13),
  1H(367,367),U(367),X(367),Y(367),Z(367),
  2NE(691,4),XX(100),YY(100),ZZ(100),AE(691)

```

```

COMMON H,U,MP,X,Y,Z,NE,XX,YY,ZZ,I,J,K,L,A,B,AE
A=0.D00
B=0.D00
BP=0.D00
W(1)=-0.5626000000000000
W(2)=.5208333333333333
W(3)=W(2)
W(4)=W(2)
CHI(1)=.3333333333333333
CHI(2)=.6000000000000000
CHI(3)=.2000000000000000
CHI(4)=CHI(3)
ETA(1)=CHI(1)
ETA(2)=CHI(3)
ETA(3)=CHI(2)
ETA(4)=CHI(3)
DO 500 II=1,4
  IF (K.EQ.1) THEN
    F(II)=CHI(II)
  ELSEIF (K.EQ.2) THEN
    F(II)=ETA(II)
  ELSE
    F(II)=1.D00-ETA(II)-CHI(II)
  ENDIF
  A1=(X(NE(J,1))*CHI(II)+X(NE(J,2))*ETA(II)+X(NE(J,3))
  $*(1.D00-CHI(II)-ETA(II))-X(I))
  B1=(Y(NE(J,1))*CHI(II)+Y(NE(J,2))*ETA(II)+Y(NE(J,3))
  $*(1.D00-CHI(II)-ETA(II))-Y(I))
  C1=(Z(NE(J,1))*CHI(II)+Z(NE(J,2))*ETA(II)+Z(NE(J,3))
  $*(1-CHI(II)-ETA(II))-Z(I))
  R=DSQRT(A1**2+B1**2+C1**2)
  BPRM31=W(II)*(F(II)-1.D00)*(1.D00/R)
  BP=BP+BPRM31
500 CONTINUE
  P1P2=DSQRT((X(NE(J,1))-X(NE(J,2)))**2+
  $(Y(NE(J,1))-Y(NE(J,2)))**2+(Z(NE(J,1))-Z(NE(J,2)))**2)
  P1P3=DSQRT((X(NE(J,1))-X(NE(J,3)))**2+
  $(Y(NE(J,1))-Y(NE(J,3)))**2+(Z(NE(J,1))-Z(NE(J,3)))**2)
  P2P3=DSQRT((X(NE(J,2))-X(NE(J,3)))**2+
  $(Y(NE(J,2))-Y(NE(J,3)))**2+(Z(NE(J,2))-Z(NE(J,3)))**2)
  IF (K.EQ.1) THEN
    BS=DABS(P1P3)
  ELSEIF (K.EQ.2) THEN
    BS=DABS(P1P2)
  ELSE
    BS=DABS(P2P3)
  ENDIF
  XXX1=0.D00
  YYY2=0.D00
  XXX2=BS
  IF (K.EQ.1) THEN
    BSS=DABS(P1P2)
  ELSEIF (K.EQ.2) THEN
    BSS=DABS(P2P3)

```

```

ELSE
  BSS=DABS(P1P3)
ENDIF
IF(K.EQ.1) THEN
  BSSS=DABS(P2P3)
ELSEIF(K.EQ.2) THEN
  BSSS=DABS(P1P3)
ELSE
  BSSS=DABS(P1P2)
ENDIF
THETA1=DACOS((BS**2+BSS**2-BSSS**2)/(2.D00*BS*BSS))
YYY3=BSS*DSIN(THETA1)
XXX3=BSS*DCOS(THETA1)
QSQS=DABS(XXX3-XXX2)
IF(QSQS.LT.0.0001) THEN
  PREBS=BSS
  BSS=BS
  BS=PREBS
  XXX2=BS
  YYY3=BSS*DSIN(THETA1)
  XXX3=BSS*DCOS(THETA1)
ELSE
  CONTINUE
ENDIF
EM=(YYY3-YYY2)/(XXX3-XXX2)
BB=-EM*BS
2121 ALP1=(1.D00/(DSQRT(1.D00+EM**2)))
ALP2=(-EM/(DSQRT(1.D00+EM**2)))
TNALF2=ALP2/(1.D00+ALP1)
TNHT1=DSIN(THETA1)/(1.D00+DCOS(THETA1))
B3NUMR=(TNHT1+TNALF2)/(1.D00-TNHT1*TNALF2)
BSTR3=((BB/(DSQRT(1.D00+EM**2)))*DLOG(DABS(B3NUMR/TNALF2)))
B=(AE(J)*BP)+(BSTR3)
RETURN
END

```

C  
C  
C

```

SUBROUTINE INTERGQ
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION W(13),ETA(13),CHI(13),F(13),
1H(367,367),U(367),X(367),Y(367),Z(367),
2NE(691,4),XX(100),YY(100),ZZ(100),AE(691)
COMMON H,U,MP,X,Y,Z,NE,XX,YY,ZZ,I,J,K,L,A,B,AE
A=0.0
B=0.0
W(1)=-0.5626000000000000
W(2)=.5208333333333333
W(3)=W(2)
W(4)=W(2)
CHI(1)=.3333333333333333
CHI(2)=.6000000000000000
CHI(3)=.2000000000000000
CHI(4)=CHI(3)

```

```

ETA(1)=CHI(1)
ETA(2)=CHI(3)
ETA(3)=CHI(2)
ETA(4)=CHI(3)
DO 400 II=1,4
  IF(K.EQ.1) THEN
    F(II)=CHI(II)
  ELSEIF (K.EQ.2) THEN
    F(II)=ETA(II)
  ELSE
    F(II)=1.-ETA(II)-CHI(II)
  ENDIF
  A1=(X(NE(J,1))*CHI(II)+X(NE(J,2))*ETA(II)+X(NE(J,3))
  $*(1-CHI(II)-ETA(II))-XX(I))
  B1=(Y(NE(J,1))*CHI(II)+Y(NE(J,2))*ETA(II)+Y(NE(J,3))
  $*(1-CHI(II)-ETA(II))-YY(I))
  C1=(Z(NE(J,1))*CHI(II)+Z(NE(J,2))*ETA(II)+Z(NE(J,3))
  $*(1-CHI(II)-ETA(II))-ZZ(I))
  R=DSQRT(A1**2+B1**2+C1**2)
  IF(L.EQ.1) THEN
    RNUM=A1
  ELSEIF(L.EQ.2) THEN
    RNUM=B1
  ELSE
    RNUM=C1
  ENDIF
  FF=F(II)*(RNUM/R**3)*W(II)
  B=B+FF
  AY1=Y(NE(J,1))-B1-YY(I)
  AY2=Y(NE(J,2))-B1-YY(I)
  AZ1=Z(NE(J,1))-C1-ZZ(I)
  AZ2=Z(NE(J,2))-C1-ZZ(I)
  AX1=X(NE(J,1))-A1-XX(I)
  AX2=X(NE(J,2))-A1-XX(I)
  A2=AY1*AZ2-AZ1*AY2
  B2=AZ1*AX2-AX1*AZ2
  C2=AX1*AY2-AY1*AX2
  GG1=DSQRT(A2**2+B2**2+C2**2)
  IF(L.EQ.1) THEN
    CF1=A2
  ELSEIF(L.EQ.2) THEN
    CF1=B2
  ELSE
    CF1=C2
  ENDIF
  T1=1./(R**3*GG1)
  T3=T1**2
  T6=A1*A2+B1*B2+C1*C2
  G=F(II)*W(II)*((-3*RNUM*R*GG1*T6*T3)+(CF1*T1))
  A=A+G
400 CONTINUE
A=AE(J)*A
B=AE(J)*B
RETURN

```

END

C  
C

```

SUBROUTINE EQSOL
  IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION M(367),H(367,367),U(367)
  COMMON H,U,MP,X,Y,Z,NE,XX,YY,ZZ,I,J,K,L,A,B
  DO 5 II=1,MP
    M(II)=1
    AMAX=H(II,1)
    DO 2 JJ=2,MP
      IF(DABS(H(II,JJ)).LE.DABS(AMAX)) GOTO 2
100  AMAX=H(II,JJ)
      M(II)=JJ
    2 CONTINUE
    IF(AMAX.EQ.0) GOTO 98
    3 NN=MP+1
    DO 4 JJ=1,NN
      4 H(II,JJ)=H(II,JJ)/AMAX
      DO 5 IP=1,MP
        IF (IP.EQ.II) GOTO 5
        MMM=M(II)
        ZMULT=H(IP,MMM)
        DO 6 JJ=1,NN
          IF(JJ.NE.MMM) GOTO 9
        8 H(IP,JJ)=0.0
        GOTO 6
      9 H(IP,JJ)=H(IP,JJ)-ZMULT*H(II,JJ)
    6 CONTINUE
    5 CONTINUE
    DO 7 II=1,MP
      NO=M(II)
      7 U(NO)=H(II,NN)
    RETURN
98 PRINT 'no solution'
  STOP
  END

```

## Program TRK15.F

C THIS PROGRAM CALCULATES THE EFFICIENCY OF ASPIRATION  
C OF PARTICLES INTO AN ARBITRARY SHAPED SAMPLING INLET  
C USING BIEM TO CALCULATE THE AIR FLOW PATTERNS AND THE  
C EQUATIONS BY ALENIOUS TO PREDICT PARTICLE LOCATION AND  
C AND VELOCITY AFTER A SMALL TIME STEP HAS ELAPSED.

C  
C THE PROGRAM REQUIRES THE OUTPUT OF THE BIEM BOUNDARY  
C SOLUTION (4PTGQ.F) AS INPUT IN ORDER TO USE THE SHELL  
C SUBROUTINE TO CALCULATE INTERNAL VELOCITIES AT THE  
C PARTICLE LOCATION.

C  
C THE SIZES OF THE ARRAYS FOR THE ARRAY VARIABLES IS  
C DEPENDENT ON THE NUMBER OF NODES AND ELEMENTS USED  
C TO FORMULATE THE BOUNDARY OF THE DOMAIN.

C  
C  
C IMPLICIT REAL \*8(A-H,O-Z)  
C DIMENSION X(367),Y(367),Z(367),PHI(367)  
C \$,DPHI(367),ID(367),ICT(367),NE(693,4),AE(693)  
C COMMON UO,UI,DIN,DP,THETA1,DTA,VX,VY,VZ,XX1,YY1,ZZ1,  
C \$NCAP,XX,YY,ZZ,MP,X,Y,Z,NE,I,J,K,L,A,B,AE,XDIN,  
C \$PHI,DPHI,ID,ICT,N,M

C  
C \*\*\*\*\*

## C INPUT VARIABLES:

C UO = WIND VELOCITY, CM/SEC  
C DP = PARTICLE DIAMETER, CM  
C DIN = INLET DIAMETER, CM  
C DTA = INITIAL TIME STEP, SEC  
C THETA1 = ANGLE OF MISALIGNMENT, DEGREES  
C UI = INLET SAMPLING VELOCITY, CM/SEC  
C XDIN = NUMBER OF INLET DIAMETERS AWAY FROM FACE  
C FOR TRAJECTORY START PTS  
C N = NUMBER OF NODES  
C M = NUMBER OF ELEMENTS  
C X,Y,Z = COORDINATES OF NODES  
C PHI, DPHI = VALUE OF POTENTIAL OR NORMAL DERIVATIVE  
C 0 IF UNKNOWN  
C ID, ICT = BOUNDARY CODES, SEE 4PTGQ.F  
C NE = ARRAY NAME FOR ALL THE TRIANGULAR ELEMENTS. EACH  
C ELEMENT IS IDENTIFIED BY THE NODE NUMBER OF  
C EACH CORNER LISTED IN A CLOCKWISE DIRECTION  
C LOOKING OUT OF THE DOMAIN. A FOURTH INTERGER  
C IN THIS ARRAY SPECIFIES WHETHER POTENTIAL OF  
C VELOCITY IS KNOWN OVER THE ELEMENT.

C X,Y,Z,PHI,DPHI,ID, AND ICT CORRESPOND TO THE OUTPUT OF  
C THE BIEM BOUNDARY SOLUTION FROM 4PTGQ.

C \*\*\*\*\*

C  
C READ REQUIRED INPUT DATA

```

C      READ (5,*) UO,DP,DIN,DTA,THETA1,UI,XDIN
      READ (5,*) CVC,CINC
      READ (5,*) N
      READ (5,*) M
      DO 1001 I=1,N
      READ (5,*) X(I), Y(I), Z(I), PHI(I), DPHI(I), ID(I),
$ICT(I)
1001  CONTINUE
      READ (5,*)((NE(I,II),II=1,4),I=1,M)
      THETA=THETA1*.017453292

C
C
C      THE J LOOP CONTAINS THE SUMMATIONS OVER EACH ELEMENT
C      INITIALLY THE AREA OF THE JTH ELEMENT IS CALCULATED
C      THIS IS AE(J).
C
      DO 200 J=1,M
      DY21=Y(NE(J,2))-Y(NE(J,1))
      DY31=Y(NE(J,3))-Y(NE(J,1))
      DZ21=Z(NE(J,2))-Z(NE(J,1))
      DZ31=Z(NE(J,3))-Z(NE(J,1))
      DX21=X(NE(J,2))-X(NE(J,1))
      DX31=X(NE(J,3))-X(NE(J,1))
      AE1=DY21*DZ31-DZ21*DY31
      AE2=DZ21*DX31-DX21*DZ31
      AE3=DX21*DY31-DY21*DX31
      AE(J)=0.5*(DSQRT(AE1**2+AE2**2+AE3**2))
200  CONTINUE

C      CALCULATE FIRST STARTING POINT
C
      NCAP=0
      NTRAJ=0
      XX=XDIN*DIN*COS(THETA1*(-1))
      YY=0.0
      ZZ=XDIN*DIN*SIN(THETA1*(-1))
250  CONTINUE
      NTRAJ=NTRAJ+1
      IF (NTRAJ.EQ. 15) THEN
      PRINT *, "first Capture not found", NTRAJ
      GOTO 3000
      ENDIF
      CALL TRAJ

C
C      CHECK FOR FIRST CAPTURE
C
      IF (NCAP.EQ. 1) THEN
      GOTO 1000
      ELSE IF ((NCAP.EQ. 2) .AND. (ZZ.GT. 0.0)) THEN
      XX=XX1-(CINC*SIN(THETA1))
      YY=0.0
      ZZ=ZZ1-(CINC*COS(THETA1))
      GOTO 250

```

```

ELSE
  XX=XX1+(CINC*SIN(THETA1))
  YY=0.0
  ZZ=ZZ1+(CINC*COS(THETA1))
  GOTO 250
ENDIF
1000 PRINT *, "NO. OF TRAJ FCAP =",NTRAJ
C
C BEGIN CRITICAL TRAJECTORY CALCULATIONS
C
XFCAP=XX1
YFCAP=YY1
ZFCAP=ZZ1
PRINT *, "1st cap:",",",",xfcap,",",",yfcap,",",",zfcap
XCAP=XX1
YCAP=YY1
ZCAP=ZZ1
C
C STEP = NUMBER OF DEGREES BETWEEN RAYS ON SEMICIRCLE
C OF STARTING POINTS, NSTEP = NUMBER OF STEPS
C
STEP=15.
NSTEP=13
nsum=35
NCOUNT=0
C
C INITIAL CAPTURE TRAJECTORY HAS BEEN FOUND, THIS SECTION OF
THE PROGRAM CALCULATES TRAJECTORY STARTING POINTS AT SUCCESSIVE
C LOCATIONS AROUND A SEMICIRCLE ABOUT THE COORDINATES OF THE
C FIRST CAPTURE
C
DO 3000 JJ=1,NSTEP
  NCOUNT=NCOUNT+1
  theta2=(-90+((ncount-1)*step))*0.017453292
  AA=.67*XDIN*DIN
  XX=XFCAP+(AA*SIN(THETA2)*SIN(THETA1))
  YY=(AA*COS(THETA2))*(-1)
  ZZ=ZFCAP+(AA*SIN(THETA2)*COS(THETA1))
  XCAP=XFCAP
  YCAP=YFCAP
  ZCAP=ZFCAP
  NFMIS=0
C
C ONCE A START POINT IS CALCULATED, THE KK LOOP PLOTS
C SUCCESSIVE TRAJECTORIES UNTIL THE CONVERGENCE CRITERIA
C IS SATISFIED.
C
DO 2900 KK=1,NSUM
1500 CALL TRAJ
  IF ((NFMIS .EQ. 0) .AND. (NCAP .EQ. 1)) THEN
    AA=CINC+AA
    XX=XFCAP+(AA*SIN(THETA2)*SIN(THETA1))
    YY=(AA*COS(THETA2))*(-1)

```

```

ZZ=ZFCAP+(AA*SIN(THETA2)*COS(THETA1))
GOTO 1500
ELSE
  NFMISS=1
ENDIF
IF (NCAP .EQ. 2) THEN
  XMISS=XX1
  YMISS=YY1
  ZMISS=ZZ1
ELSE
  XCAP=XX1
  YCAP=YY1
  ZCAP=ZZ1
ENDIF

C
C   S IS THE DISTANCE BETWEEN THE LAST CAPTURE AND LAST
C   MISS. S IS COMPARED TO CVC AND LOOP EXITED IF S < CVC.
C
$  S=SQRT((XCAP-XMISS)**2+(YCAP-YMISS)**2+
      (ZCAP-ZMISS)**2)
  IF (S .LT. CVC) THEN
    GOTO 2990
  ELSE
    XX=(XMISS+XCAP)/2
    YY=(YMISS+YCAP)/2
    ZZ=(ZMISS+ZCAP)/2
  ENDIF
  if (kk .eq. nsum) print *, "no convergence, s =",s
2900 CONTINUE
2990 XCRIT=(XMISS+XCAP)/2
      YCRIT=(YMISS+YCAP)/2
      ZCRIT=(ZMISS+ZCAP)/2

C
C   EACH CRITICAL TRAJECTORY COORDINATE IS WRITTEN TO THE
C   OUTPUT UNIT.
C
  write (6,*)"crit",",",",ncount",",",",xcrit",",",",ycrit",",",",zcrit
3000 CONTINUE
  STOP
  END

C
C
C
C   SUBROUTINE TRAJ
C
C   THIS SUBROUTINE TAKES A SINGLE PARTICLE STARTING
C   POINT, ASSIGNS THE INITIAL VELOCITY VALUES TO THE
C   PARTICLE, AND TRACKS THE PARTICLE TO THE FACE OF THE
C   INLET (CAPTURE) OR OUT OF THE BOUNDARY (MISS)
C
  IMPLICIT REAL *8(A-H,O-Z)
  DIMENSION VXOL(1600),VYOL(1600),VZOL(1600),
1X(367),Y(367),Z(367),PHI(367),DPHI(367),ID(367)
2,ICT(367),NE(693,4),AE(693)

```

```
COMMON UO,UI,DIN,DP,THETA1,DTA,VX,VY,VZ,XX1,YY1,ZZ1,
$NCAP,XX,YY,ZZ,MP,X,Y,Z,NE,I,J,K,L,A,B,AE,XDIN,
$PHI,DPHI,ID,ICT,N,M
```

```
C
C  print *, M
C  G=-980.
C  DT=DTA
C  AV=.000183
C  PDENS=1.0
C  ADENS=.001205
C  DPL=10000.0*DP
C  CC=1+((2.*0.07/DPL)*(1.257+(0.4*EXP(-0.55*DPL/0.07))))
C  TAU=(DP**2*PDENS*CC)/(18*AV)
C  GX=G*SIN(THETA1)
C  GZ=G*COS(THETA1)
C  GY=0
C
C
C  MANY=9999
C  NCAP=0
C  N1=1
C  DO 4300 I=1,MANY
C      CALL SHELL
C      IF (I .EQ. 1) THEN
C          VXNOW=VX+(TAU*GX)
C          VYNOW=VY+(TAU*GY)
C          VZNOW=VZ+(TAU*GZ)
C          XX1=XX
C          YY1=YY
C          ZZ1=ZZ
C      ENDIF
C      VR=((VXNOW-VX)**2+(VZNOW-VZ)**2
$      +(VYNOW-VY)**2)**0.5
C      RE=VR*DP*ADENS/AV
C      IF (RE .LE. 0.5) THEN
C          QRE=1
C      ELSE IF ((RE .GT. 0.5) .AND. (RE .LE. 800.)) THEN
C          QRE=1+(0.15*RE**0.687)
C      ELSE
C          QRE=0.44*RE/24
C      ENDIF
C      IF (I .EQ. 1) THEN
C          VXOL(I)=VX
C          VYOL(I)=VY
C          VZOL(I)=VZ
C      ELSE
C          VXOL(I)=VXOL(I-1)
C          VZOL(I)=VZOL(I-1)
C          VYOL(I)=VYOL(I-1)
C      ENDIF
$      if ((XX .lt. 1.5*din) .and. (XX .gt. (-1.5)*din)
$      .and. (YY .lt. 1.5*din) .and. (YY .gt. (-1.5)*din)
$      .AND. (ZZ .LT. 1.5*DIN) .AND. (ZZ .GT. (-1.5)*DIN))
$      then
```

```

        DT=DTA/2.
    else
        DT=DTA
    endif
    UAX=(VX-VXOL(I))/DT
    UAZ=(VZ-VZOL(I))/DT
    UAY=(VY-VYOL(I))/DT
    UBX=VX-((UAX-GX)*(TAU/QRE))
    UBY=VY-((UAY-GY)*(TAU/QRE))
    UBZ=VZ-((UAZ-GZ)*(TAU/QRE))
    VXNEW=(UAX*DT)+UBX-((UBX-VXNOW)*
$      EXP(-QRE*DT/TAU))
    VYNEW=(UAY*DT)+UBY-((UBY-VYNOW)*
$      EXP(-QRE*DT/TAU))
    VZNEW=(UAZ*DT)+UBZ-((UBZ-VZNOW)*
$      EXP(-QRE*DT/TAU))
    XXNEW=XX+(UAX/2*DT**2)+(UBX*DT)-
$      ((UBX-VXNOW)*(TAU/QRE)*(1-EXP(-QRE*DT/TAU)))
    ZZNEW=ZZ+(UAZ/2*DT**2)+(UBZ*DT)-
$      ((UBZ-VZNOW)*(TAU/QRE)*(1-EXP(-QRE*DT/TAU)))
    YYNEW=YY+(UAY/2*DT**2)+(UBY*DT)-
$      ((UBY-VYNOW)*(TAU/QRE)*(1-EXP(-QRE*DT/TAU)))
    IF (XXNEW .LT. (-1.1)*XDIN/2*DIN) THEN
        NCAP=2
    c      PRINT *, 'PARTICLE EXIT REAR BOUNDARY, MISS'
        GOTO 4301
    ELSE IF ((ZZNEW .GT. 1.1*XDIN*DIN) .OR. (ZZNEW .LT.
$      (-1.1)*XDIN*DIN)) THEN
        NCAP=2
    c      PRINT *, 'PARTICLE EXIT TOP/BOTTOM, MISS'
        GOTO 4301
    ELSE IF ((YYNEW .GT. 1.1*XDIN*DIN) .OR. (YYNEW .LT.
$      (-1.1)*XDIN*DIN)) THEN
        NCAP=2
    c      PRINT *, 'PARTICLE EXIT SIDE, MISS'
        GOTO 4301
    ELSE IF ((XXNEW .LT. 0.05*din) .AND. (XX .GT.
$      0.05*din)
$      .AND. (ABS(ZZNEW) .LT. DIN/2+.05) .AND.
$      (ABS(YYNEW) .LT. DIN/2+.05)) THEN
        NCAP=1
    c      PRINT *, 'CAPTURE AT FACE'
        GOTO 4301
    ELSE IF ((ABS(ZZNEW) .LT. DIN/2+.05) .AND.
$      (ABS(YYNEW) .LT. DIN/2+.05) .AND.
$      (XXNEW .LT. 0.0))
$      THEN
        NCAP=2
    c      PRINT *, 'CONTACT TUBE, MISS'
        GOTO 4301
    ELSE
        NCAP=0
    ENDIF
    N1=N1+1

```

```

      XX=XXNEW
      YY=YYNEW
      ZZ=ZZNEW
      VXNOW=VXNEW
      VYNOW=VYNEW
      VZNOW=VZNEW
4300  CONTINUE
4301  RETURN
      END

C
C
C
      SUBROUTINE SHELL
C
C THIS SUBROUTINE CALCULATES THE INTERNAL AIR VELOCITY
C COMPONENTS IN 3 DIMENSIONS AT THE LOCATION THAT THE PARTICLE
C IS LOCATED USING THE BIEM INTERNAL SOLUTION ROUTINE. IT
C FURTHERCALLS SUBROUTINE INTERGQ TO PERFORM THE INTERNAL
C GAUSSIAN QUADRATURE.
C
C
      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION PREV(3),AE(693),NE(693,4),
1X(367),Y(367),Z(367),PHI(367),DPHI(367),ID(367)
2,ICT(367),ALTDPHI(693,3)
      COMMON UO,UI,DIN,DP,THETA1,DTA,VX,VY,VZ,XX1,YY1,ZZ1,
$NCAP,XX,YY,ZZ,MP,X,Y,Z,NE,I,J,K,L,A,B,AE,XDIN,
$PHI,DPHI,ID,ICT,N,M
      MP=N

C
C
C
      DECLARE AND INITIALIZE
C
      PVX=0.0
      PVY=0.0
      PVZ=0.0
      DO 2000 J=1,M
      PREVX=0.0
      PREVY=0.0
      PREVZ=0.0
      DO 3000 K=1,3
      DO 4000 L=1,3
      CALL INTERGQ
      IF (ICT(NE(J,K)).EQ.1.AND.ID(NE(J,K)).EQ.1
$ .AND.ID(NE(J,4)).EQ.2) THEN
      DPHIDE=DPHI(NE(J,4))
      ELSE
      DPHIDE=DPHI(NE(J,K))
      ENDIF
      PREV(L)=(A*PHI(NE(J,K))-B*DPHIDE)
4000  CONTINUE
      PREVX=PREVX+PREV(1)
      PREVY=PREVY+PREV(2)
      PREVZ=PREVZ+PREV(3)

```

```

3000 CONTINUE
    PVX=PVX+PREVX
    PVY=PVY+PREVY
    PVZ=PVZ+PREVZ
2000 CONTINUE
    COEF1=-0.079577471
    VX=COEF1*PVX
    VY=COEF1*PVY
    VZ=COEF1*PVZ
1100 CONTINUE
C
C
444 CONTINUE
C   CLOSE (4)
    RETURN
    END
C
C
C
    SUBROUTINE INTERGQ
    IMPLICIT REAL*8(A-H,O-Z)
    DIMENSION W(13),ETA(13),CHI(13),F(13),NE(693,4),
    1X(367),Y(367),Z(367),PHI(367),DPHI(367),ID(367),ICT(367)
    2,AE(693)
    COMMON UO,UI,DIN,DP,THETA1,DTA,VX,VY,VZ,XX1,YY1,ZZ1,
    $NCAP,XX,YY,ZZ,MP,X,Y,Z,NE,I,J,K,L,A,B,AE,XDIN,
    $PHI,DPHI,ID,ICT,N,M
    A=0.0
    B=0.0
    W(1)=.3333333333333333
    W(2)=W(1)
    W(3)=W(2)
    CHI(1)=.6666666666666667
    CHI(2)=.1666666666666667
    CHI(3)=CHI(2)
    ETA(1)=.1666666666666667
    ETA(2)=.1666666666666667
    ETA(3)=.6666666666666667
    DO 400 II=1,3
    IF(K.EQ.1) THEN
        F(II)=CHI(II)
    ELSEIF (K.EQ.2) THEN
        F(II)=ETA(II)
    ELSE
        F(II)=1.-ETA(II)-CHI(II)
    ENDIF
    A1=(X(NE(J,1))*CHI(II)+X(NE(J,2))*ETA(II)+X(NE(J,3))
    $*(1-CHI(II)-ETA(II))-XX)
    B1=(Y(NE(J,1))*CHI(II)+Y(NE(J,2))*ETA(II)+Y(NE(J,3))
    $*(1-CHI(II)-ETA(II))-YY)
    C1=(Z(NE(J,1))*CHI(II)+Z(NE(J,2))*ETA(II)+Z(NE(J,3))
    $*(1-CHI(II)-ETA(II))-ZZ)
    R=DSQRT(A1**2+B1**2+C1**2)
    IF(L.EQ.1) THEN

```

```

      RNUM=A1
    ELSEIF(L.EQ.2) THEN
      RNUM=B1
    ELSE
      RNUM=C1
    ENDIF
    FF=F(II)*(RNUM/R**3)*W(II)
    B=B+FF
    AY1=Y(NE(J,1))-B1-YY
    AY2=Y(NE(J,2))-B1-YY
    AZ1=Z(NE(J,1))-C1-ZZ
    AZ2=Z(NE(J,2))-C1-ZZ
    AX1=X(NE(J,1))-A1-XX
    AX2=X(NE(J,2))-A1-XX
    A2=AY1*AZ2-AZ1*AY2
    B2=AZ1*AX2-AX1*AZ2
    C2=AX1*AY2-AY1*AX2
    GG1=DSQRT(A2**2+B2**2+C2**2)
    IF(L.EQ.1) THEN
      CF1=A2
    ELSEIF(L.EQ.2) THEN
      CF1=B2
    ELSE
      CF1=C2
    ENDIF
    T1=1./(R**3*GG1)
    T3=T1**2
    T6=A1*A2+B1*B2+C1*C2
    G=F(II)*W(II)*((-3*RNUM*R*GG1*T6*T3)+(CF1*T1))
    A=A+G
400  CONTINUE
    A=AE(J)*A
    B=AE(J)*B
    RETURN

```

END

Program AREA.FOR

C THIS CODE CALCULATE THE AREA UNDER A CURVE USING TRAPIZOIDAL  
RULE.

C

C INPUT

C N ; NUMBER OF INPUT POINTS

C X ; X-COORD. OF THE POINT

C Y ; Y-COORD. OF THE POINT

C

C OUTPUT ---> AREA ON THE SCREEN.

C

\$DEBUG

IMPLICIT REAL\*8(A-H,O-Z)

DIMENSION X(37),Y(37)

READ (7,\*) N

DO 100 I=1,N

READ (7,\*) y(i),x(i)

100 CONTINUE

SUM=0.0

DO 200 I=1,N-1

DX=X(I+1)-X(I)

IF(DX.GT.0.000000D0) THEN

T=1.0

ELSE

T=-1.0

ENDIF

TEMP=DABS(DX)\*DABS(Y(I+1)+Y(I))/2.D0

200 SUM=SUM+T\*TEMP

write(\*,1001) SUM

1001 format(e20.5)

STOP

END

Trajectory Plotting Program in BASIC

Program PART.BAS

```
10 OPEN "filename of traj coords" FOR INPUT AS #1
20 OPEN "filename of efficiency data" FOR INPUT AS #2
30 CLS
40 SCREEN 1
50 WINDOW (-6,-12)-(12,12)
60 INPUT #2, UO,UI,DP,DIN,THETA,EFF
70 THETA = 57.29577951#*THETA
80 LINE (0,DIN/2)-(0,-DIN/2)
90 LINE (0,DIN/2)-(-6,DIN/2)
100 LINE (0,-DIN/2)-(-6,-DIN/2)
110 WHILE NOT EOF(1)
120 INPUT #1, XX,YY
130 PSET (XX,YY)
140 WEND
150 CLOSE #1
160 CLOSE #2
170 KEY OFF
180 LOCATE 19,8:PRINT "EFF = ";EFF
190 LOCATE 20,8:PRINT "UO = ";UO
200 LOCATE 21,8:PRINT "DP = ";DP
210 LOCATE 22,8:PRINT "DIN = ";DIN
220 LOCATE 23,8:PRINT "THETA = ";THETA
230 LOCATE 24,8:PRINT "UI = ";UI
240 A$=INKEY$:IF A$="C" THEN 260 ELSE 250
250 IF A$="X" THEN 270 ELSE 240
260 LPRINT CHR$(12)
270 END
```

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